

# McDeLicious Workshop

*13-14 March 2008*

S.P. Simakov

*Institut für Reaktorsicherheit,  
Forschungszentrum Karlsruhe*

## What is McDeLicious code

- McDeLicious code  
was developed to enable a proper representation of the d-Li neutron source term in Monte Carlo transport calculations for IFMIF
- It is enhancement (set of subroutines) to MCNP5 with ability to sample the generation of d-Li source neutrons on the basis of tabulated double-differential d +  $^{6,7}\text{Li}$  cross-sections:
  - modelling of deuteron beam configuration, orientation and profile
  - modelling of deuteron slowing down in the Lithium
  - sampling of source neutrons using evaluated d+  $^{6,7}\text{Li}$  data

## History of McDeLicious code development

- 1999: McDeLi (*P. Wilson, Report FZKA 6218, 1999*)
  - enhancement to MCNP-4a to sample the generation of d-Li source neutrons on the basis of embed analytical formulas representing direct deuteron stripping (Serber model) and compound reactions
- 2001: McDeLicious (*S.P.Simakov et al. J.Nucl.Mat.307-311(2002)1710, FZKA 6743*)
  - enhancement to MCNP-4b,c to sample the d-Li source neutrons on the basis of tabulated double-differential d + <sup>6,7</sup>Li cross-sections for deuteron energies up to 50 MeV  
(evaluated by *A. Konobeyev et al., NSE 139 (2001)1*)
- 2005: McDeLicious-05 – compilation with MCNP-5 and use tabulated double-differential cross-sections from updated d + <sup>6,7</sup>Li evaluation (*made by P. Pereslavytsev et al., J.Nucl.Mat.367-370(2007)1531*)

## **D-Li Neutron Source Term:**

validation against measurements  
performed at accelerators with

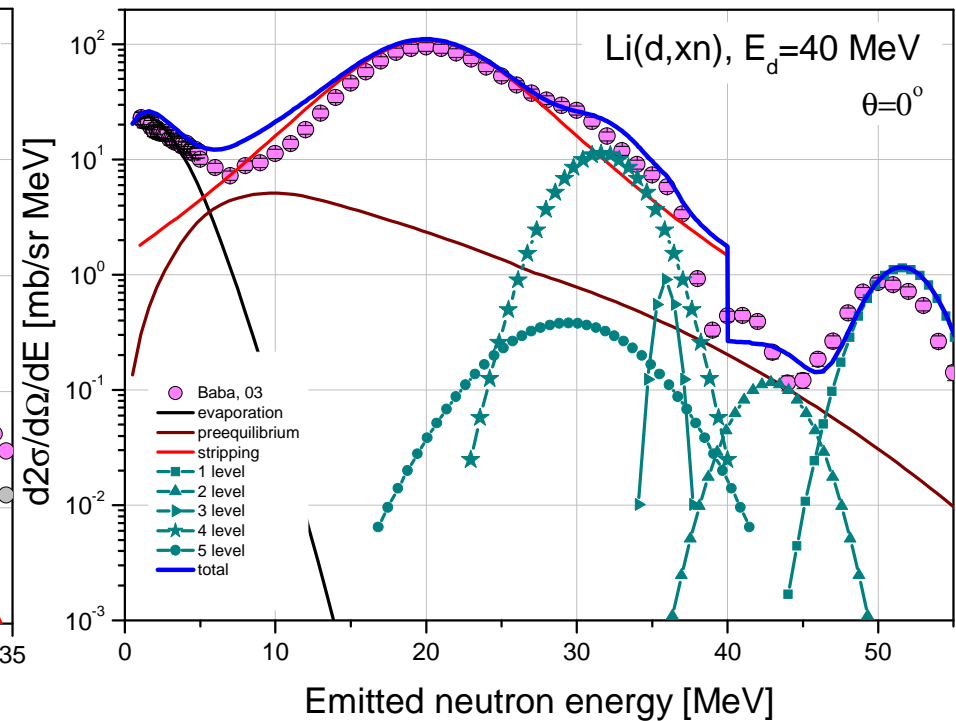
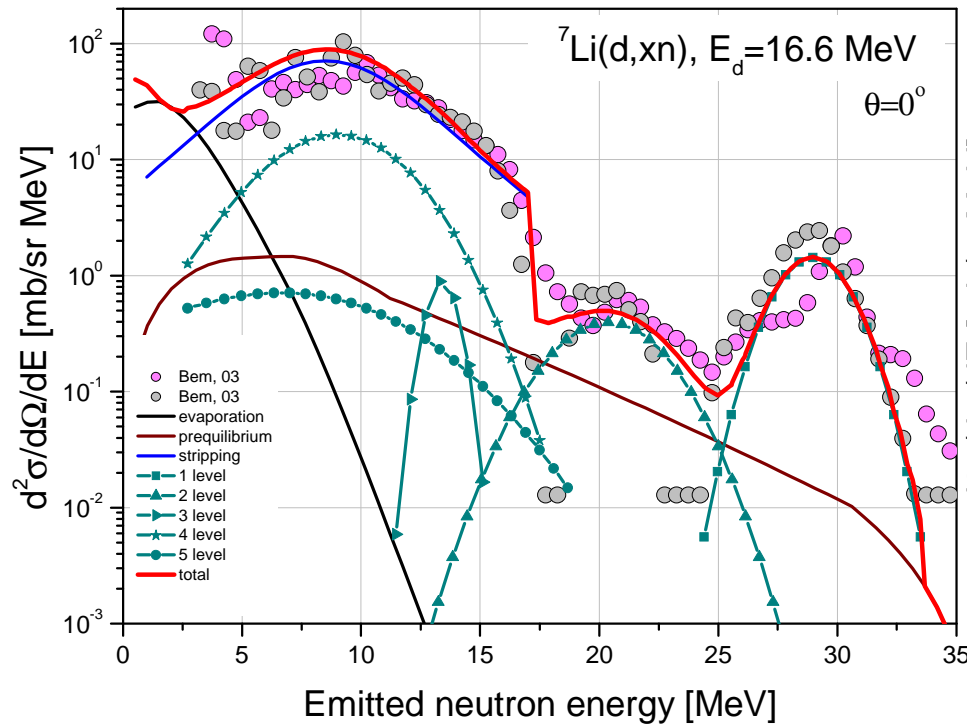
- thin Li-target - double differential cross sections
- thick Li-target - integrated & differential neutron yields

# Double differential cross sections /thin Li-target/: new measurements and new d + <sup>6,7</sup>Li data evaluation

Ed = 17 MeV

Ed = 40 MeV

Exp.: P.Bem et al. NPI EXP(EFDA)-05/2004    Exp.: M.Hagiwara et al. Fus.Sci.Tech.48(2005)1320

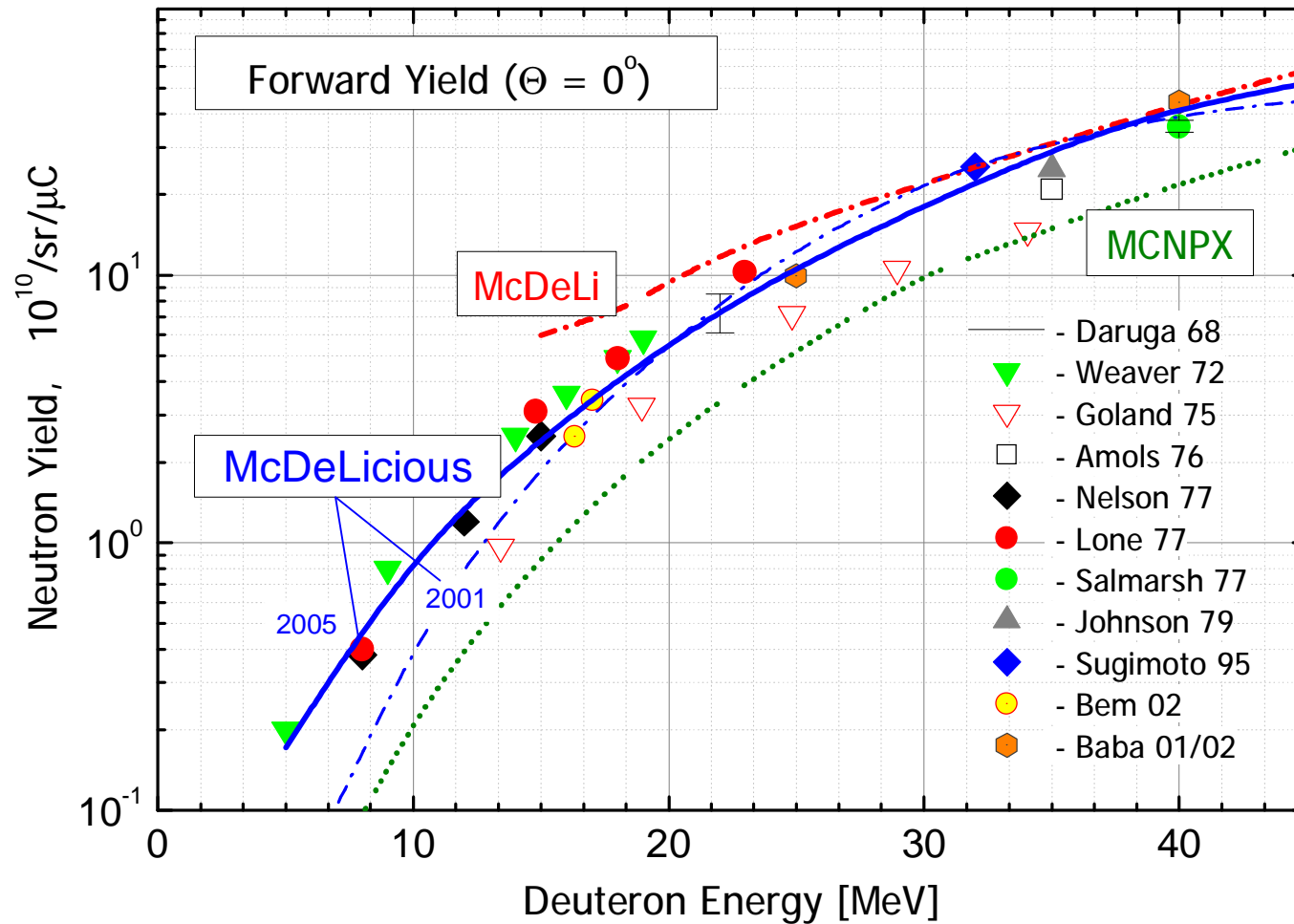


Evaluation by P. Pereslavytsev et al., JNM 367-370(2007)1531

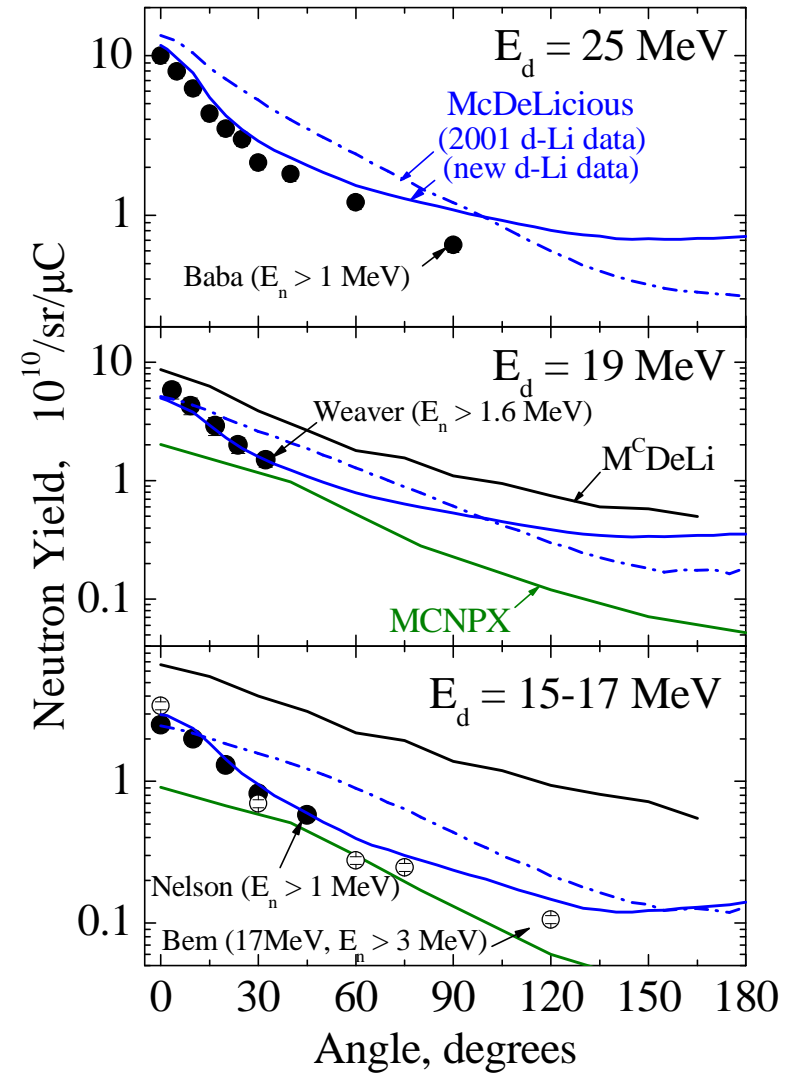
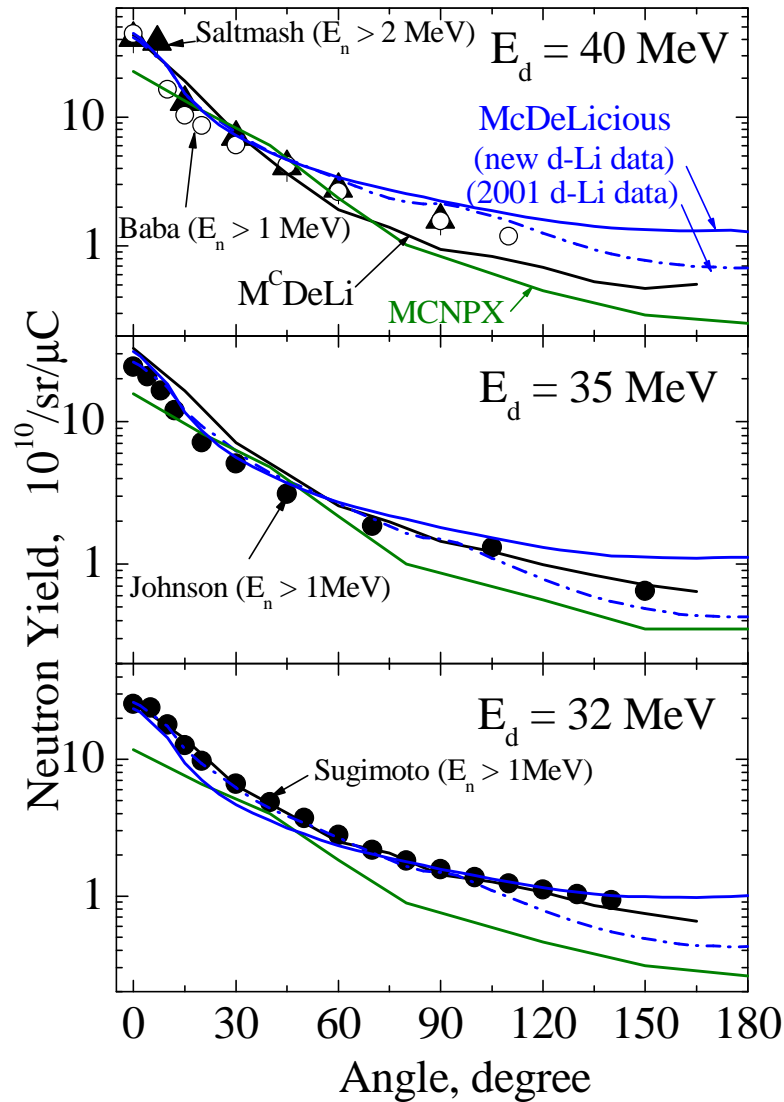
## Neutron yield from thick Li-target: available experiments

No	First Author, Year of Publ.	Laboratory, Country	Tar- get	$E_d$ , MeV	$Q$ , degrees	$E_{thr}$ , MeV
1	V.K. Daruga 1968	Inst. of Physics & Power Eng., Russia	Li	22	0°	1.8
2	A.N. Weaver 1972	Livermore Laboratory, USA	Li	5, 9, 14, 16, 19	3.5°, 10°, 18°, 25°, 32°	2.5 1.6
3	A.N. Goland 1975	Naval Research Laboratory, USA	Li	13.4, 19, 25, 29, 34	0°, 5°, 10°, 15°, 20°	3
4	H.I. Amols 1976	Fermi National Laboratory, USA	Li	35	0°	5
5	C.E. Nelson 1977	Triangle University, USA	<sup>7</sup> Li	8, 12, 15	0°, 10°, 20°, 30°, 45°	1
6	M.A. Lone 1977	Chalk River Labo- ratory, Canada	<sup>7</sup> Li	14.8, 18, 23	0°, 10°, 20°, 30°, 40°	0.3
7	M.J. Saltmarsh 1977	Oak Ridge Laboratory, USA	Li	40	0°, 7°, 15°, 30°, 45°, 60°, 90°	2
8	D.L. Johnson 1979	University of California, USA	Li	35	0°, 4°, 8°, 12°, 20°, 30°, 45°, 70°, 105°, 150°	1
9	M. Sugimoto 1995	Japan Energy Research Institute, Japan	Li	32	0°, 5°, 10°, 15°, 20°, 30°, 40°, 50°, 60°, 70°, 80°, 90°, 100°, 110°, 120°, 130°, 140°, 150°	1
10	M. Baba 2003	Tohoku University, Japan	Li	25, 40	0°, 5°, 10°, 15°, 20°, 25°, 30°, 40°, 45°, 60°, 90°, 110°	1
11	P. Bém 2003	Nuclear Physics Institute, Rez	Li	16.3, 17.0	0°	3

# Thick Li-target neutron source: Forward Neutron Yield



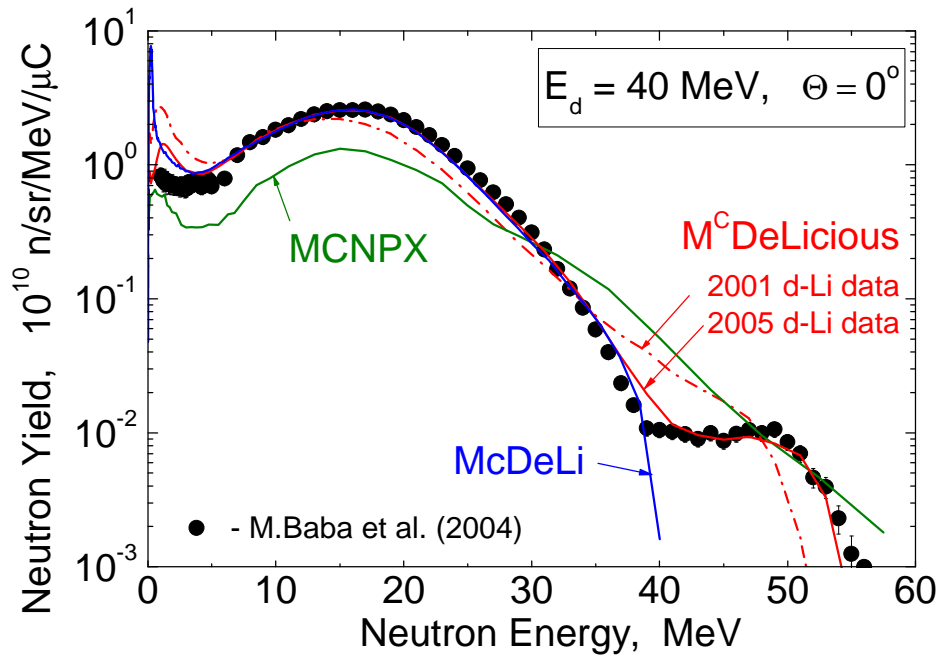
# Thick Li-target neutron source: Angular Neutron Yield



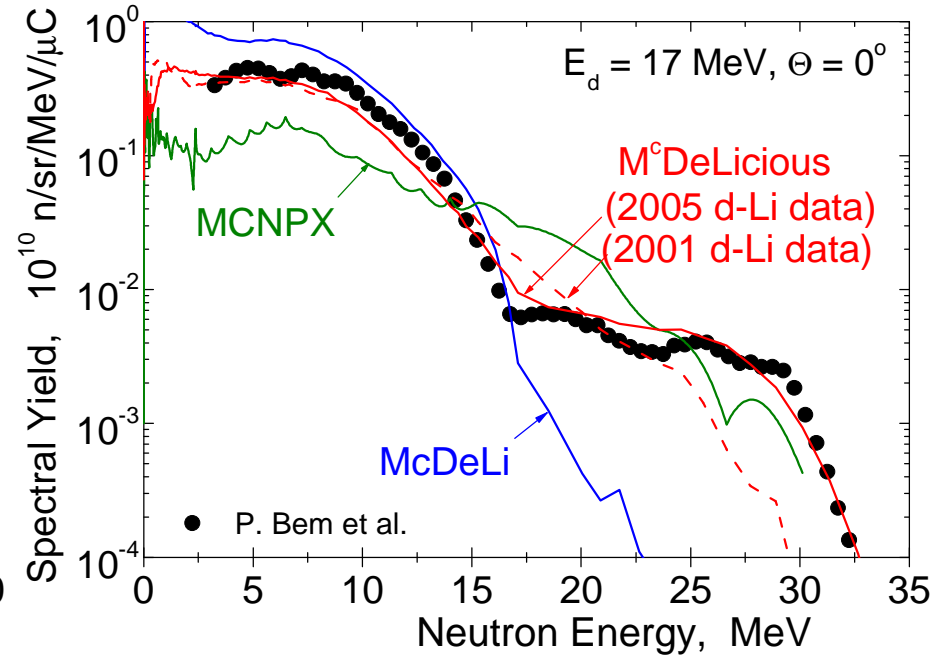


# Thick Li-target neutron source: Energy-Angular Yield

$E_d = 40$  MeV  
Exp.: M. Hagiwara et al.



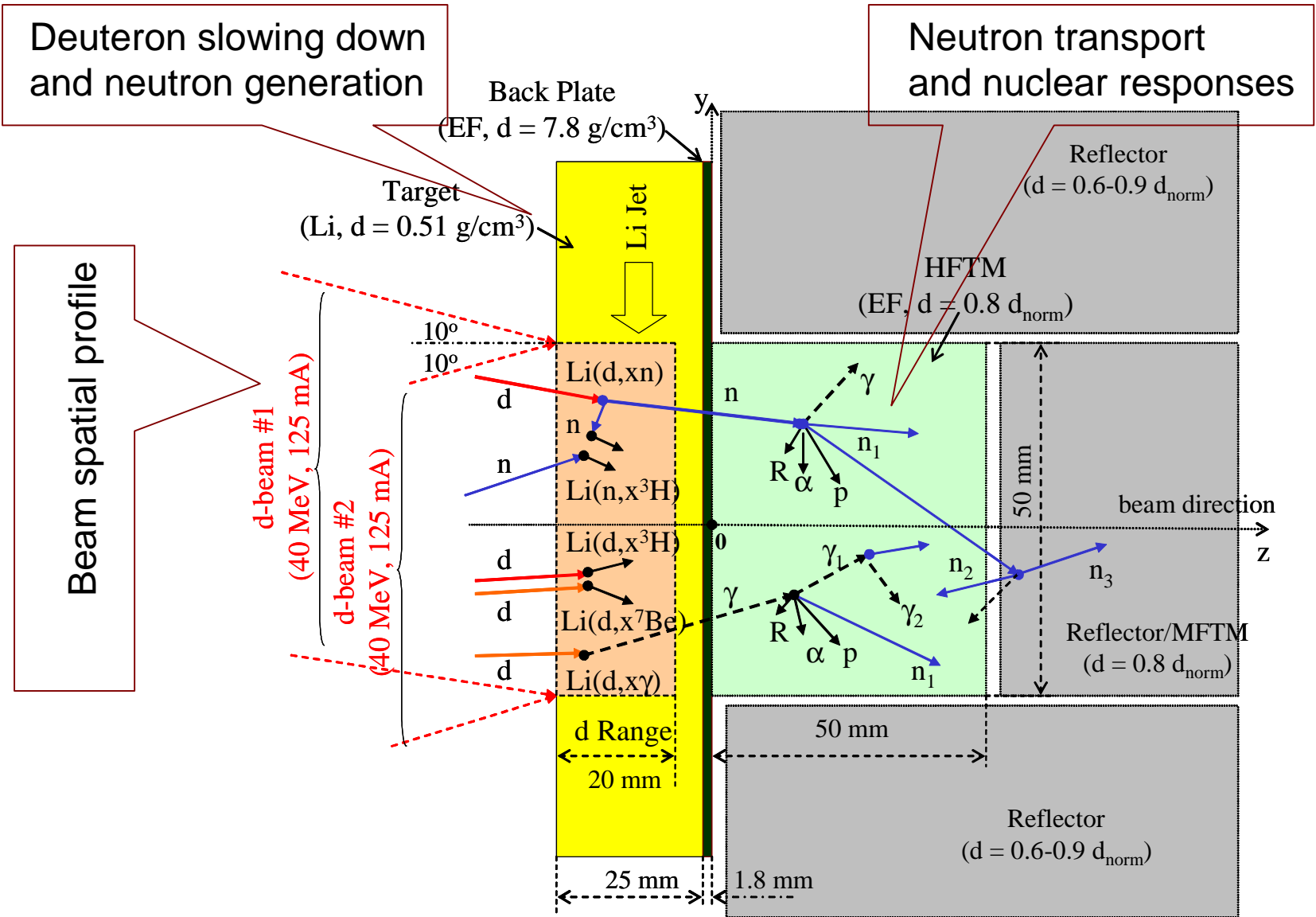
$E_d = 17$  MeV  
Exp.: P. Bem et al.



## **D-Li Neutron Source Term:**

simulation of IFMIF source

# Basic nuclear processes in IFMIF

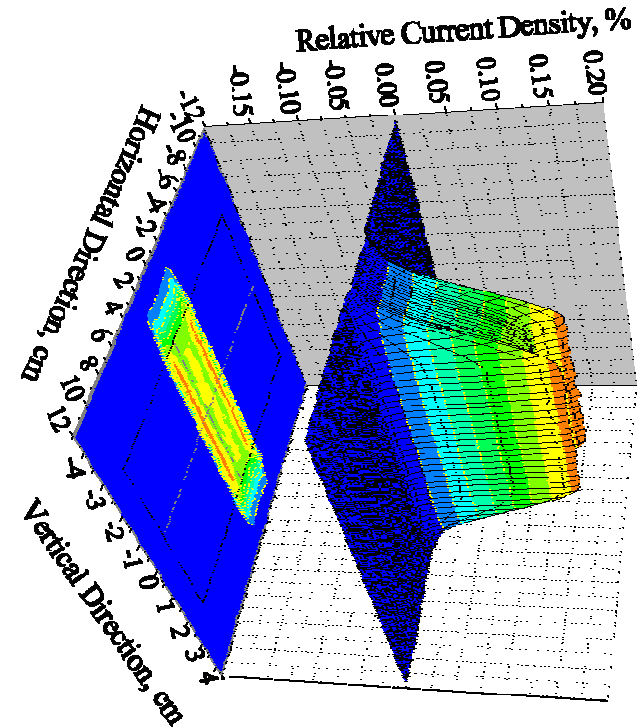
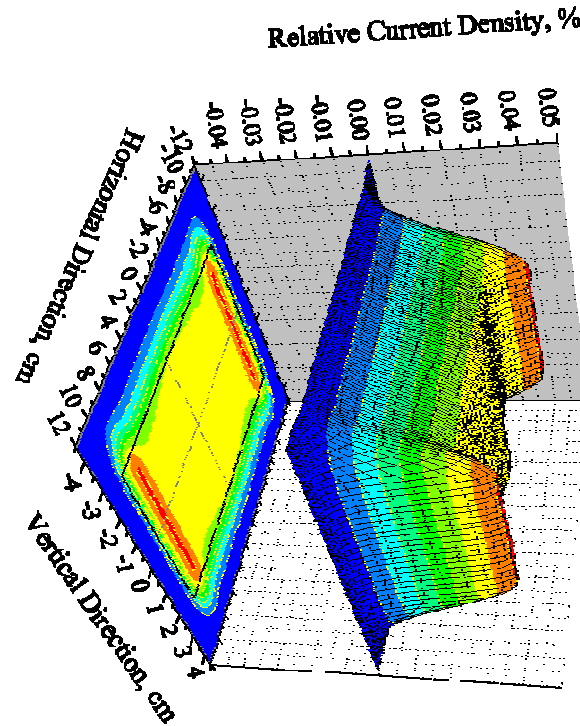


# Dual deuteron beam spatial profile: each 40MeV @125 mA

Full Footprint: 20×5 cm<sup>2</sup>

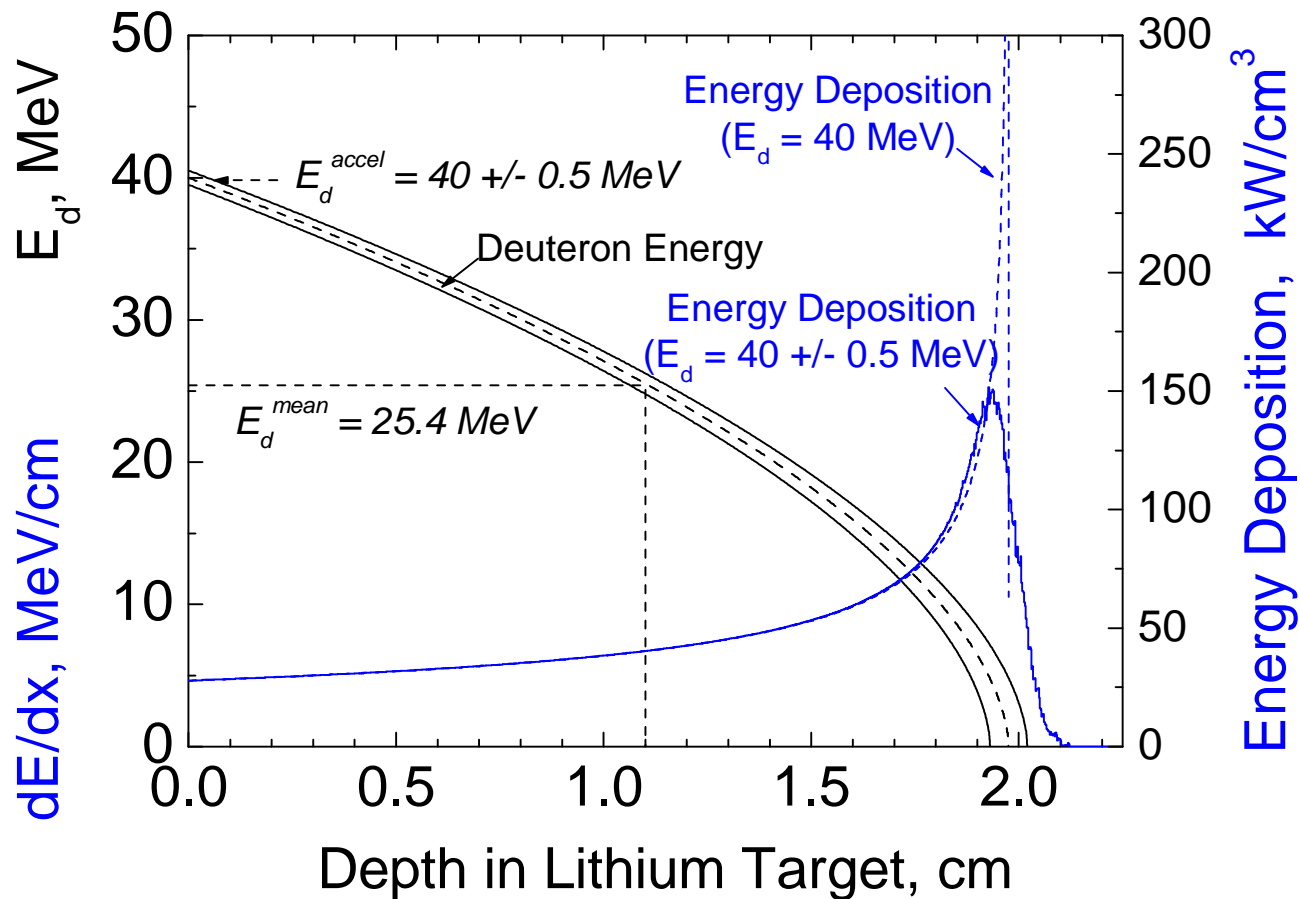
Reduced Footprint: 4×5 cm<sup>2</sup>

Two 40 MeV @ 125 mA  
beams:  
+/- 10° declination  
in horizontal plane



- d-beam current density variation inside the beam foot print amounts up to 20% ;
- d-beam current density gradient at the beam foot print edges (10 to 90)% per 1.5 cm
- d-beam current density 3-d distribution based on results *obtained ≈ 10 years ago!*

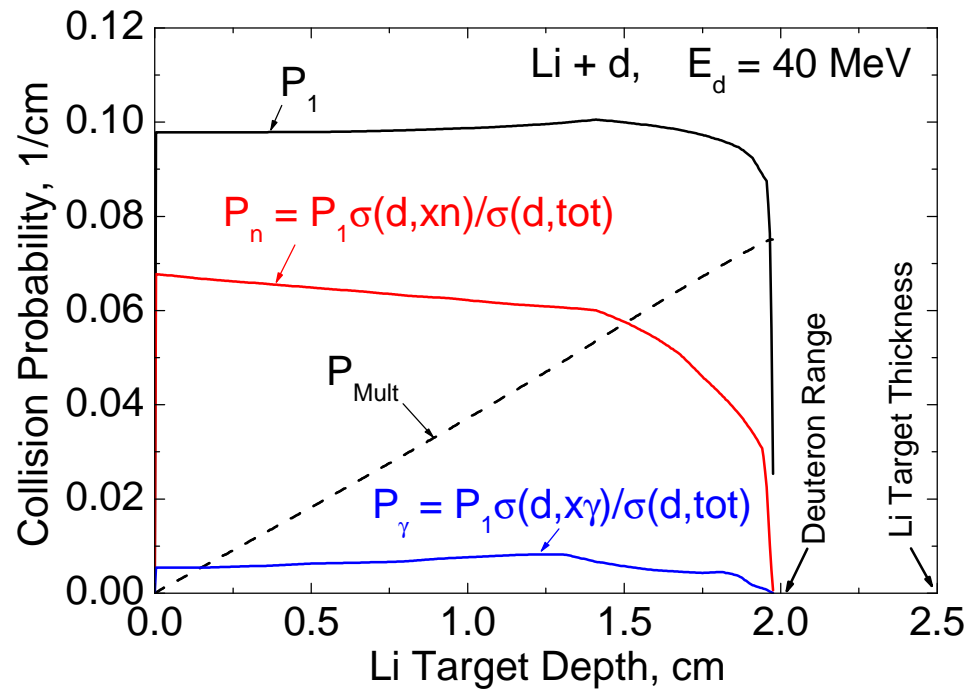
## Deuteron slowing down and energy deposition in Li-jet



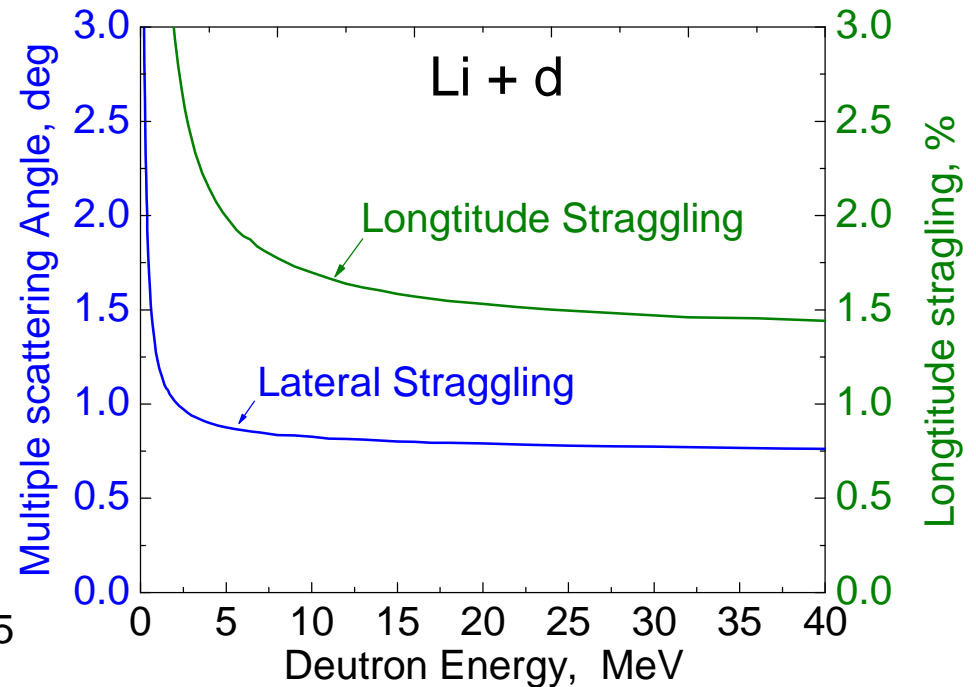
- Deuteron track length reach 2.1 cm;
- Peak Energy Deposition is 150 kW/cc at the depth of 2.0 cm (at the end of d-track)  
(without incident deuteron energy smearing - 1000 kW/cc !)
- Average energy deposition in Li jet =  $(40 \text{ MeV} \times 250 \text{ mA} = 10,000 \text{ kW}) / (20 \times 5 \times 2 \text{ cc}) = 50 \text{ kW/cc}$

# Deuteron collisions and Neutron productions probabilities in Li-jet

## Probabilities

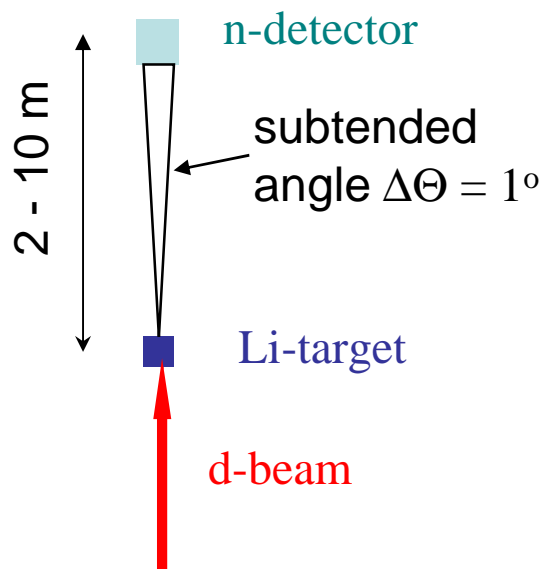


## Straggling

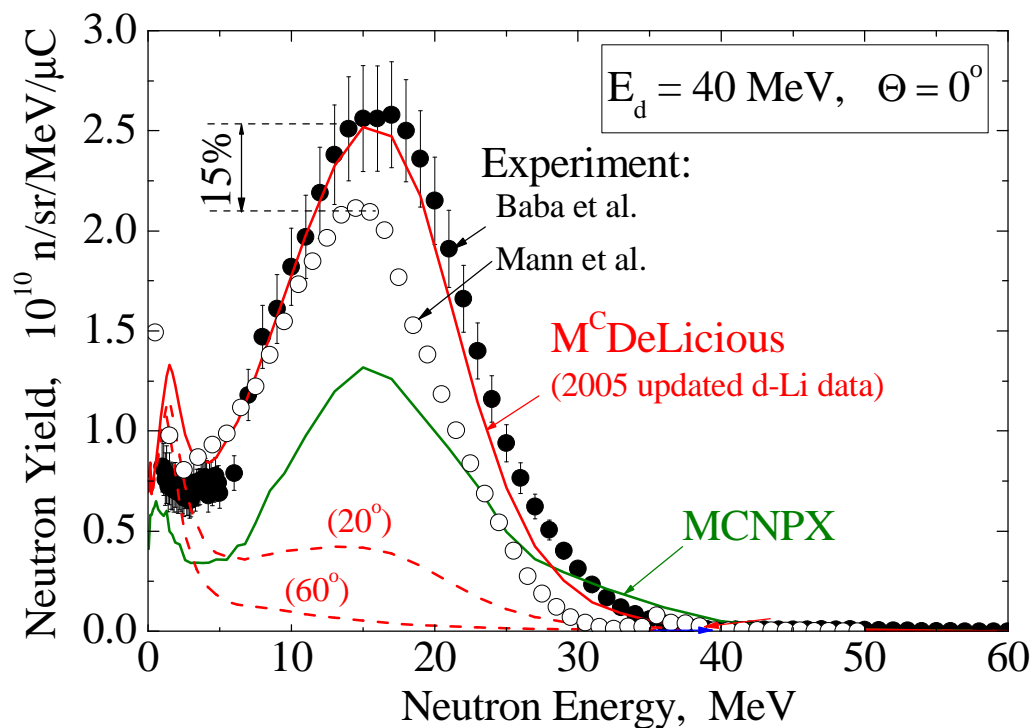


- First deuteron collision in Li-jet dominates
- Second collisions - most probably are an elastic scattering  
which conserves incident deuteron direction within  $1^\circ$  and energy
- Every 100 deuterons with 40 MeV produce in Li-jet: 7.2 neutrons and 1.2 gammas

# D-Li Neutron Spectra: thick target measurements in laboratory do show a 14 MeV peak !



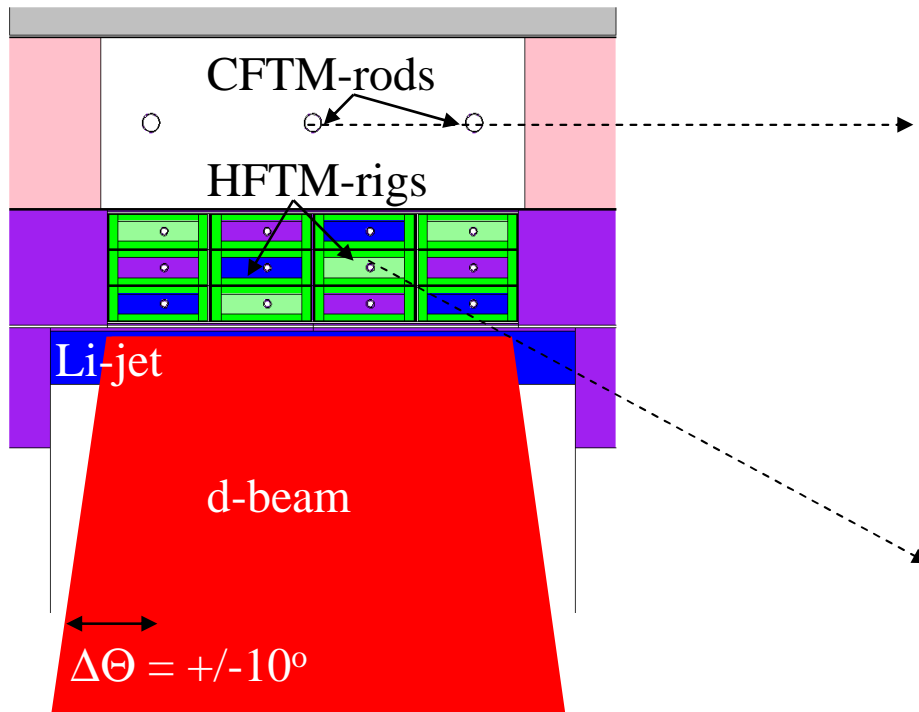
## Neutron Spectra at well defined angles:



*Peak at energy 15 MeV is clearly visible in well fine angle geometry. This peak is reproduced by 2005 updated d-Li evaluation within 10%*

# Does IFMIF neutron spectra have 14 MeV peak (?)

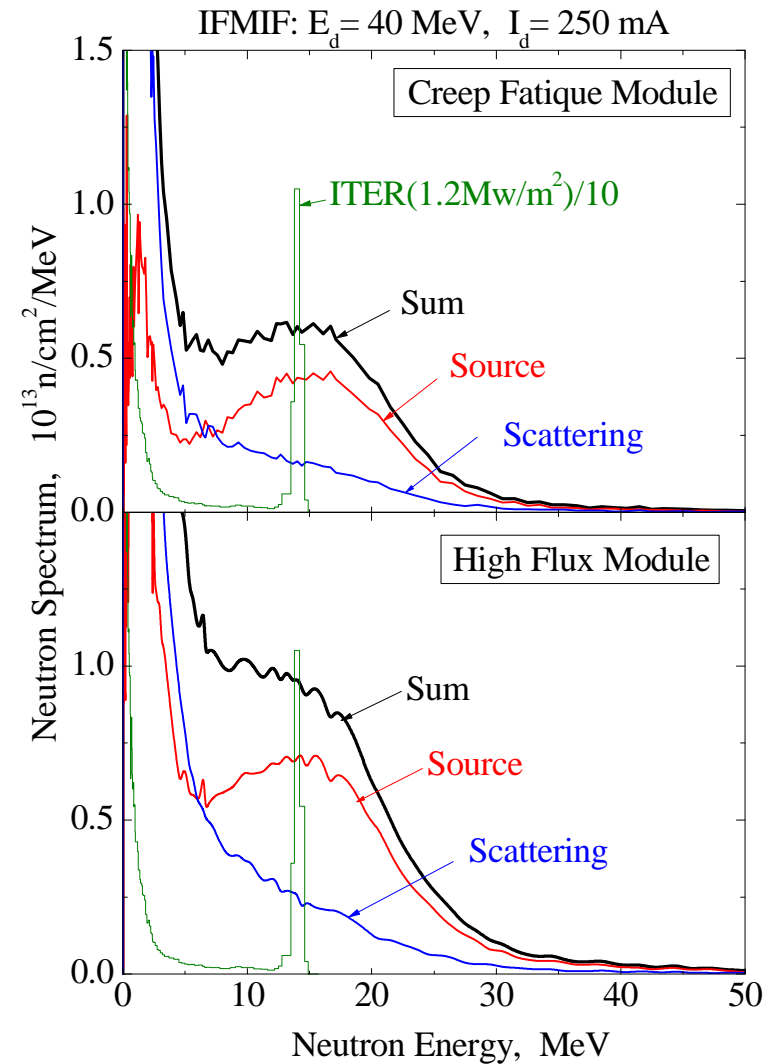
IFMIF fragment:



Angular smearing and multiple scattering smooth a 14 MeV neutron peak in HFTM, resulting to the shape without local extremes

S.P. Simakov et al. Fus.Eng.Des.82(2007)2510

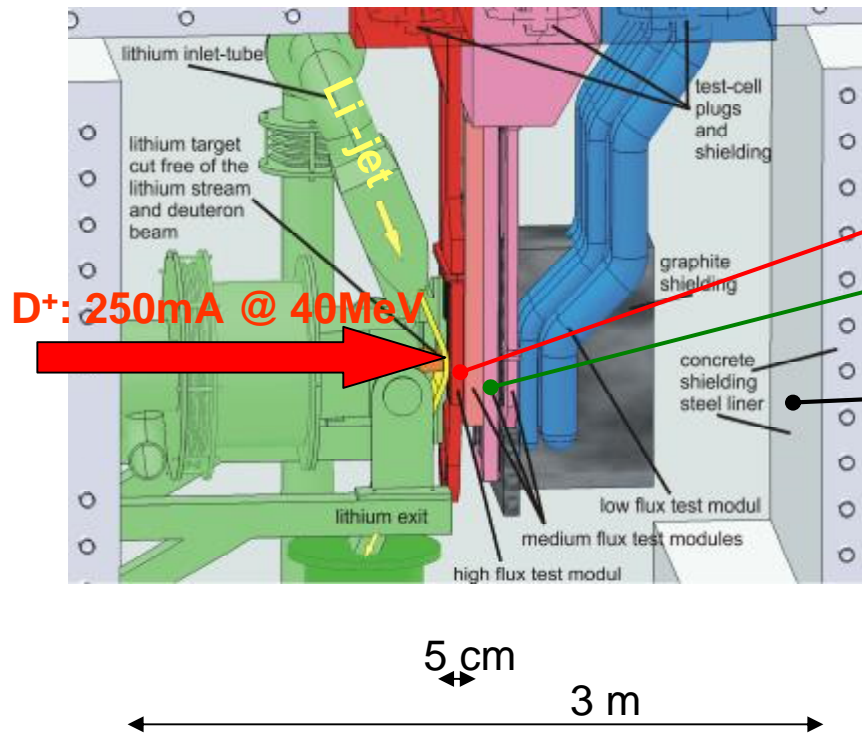
Neutron Spectra at Atom point



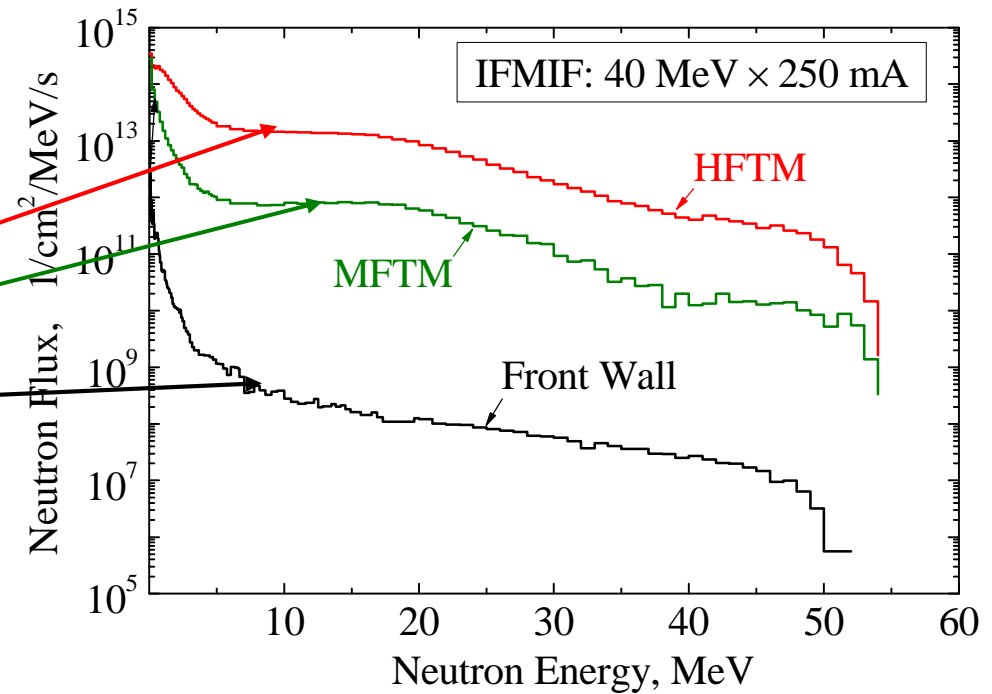


## Neutron spectra inside the Test Cell

IFMIF test cell design



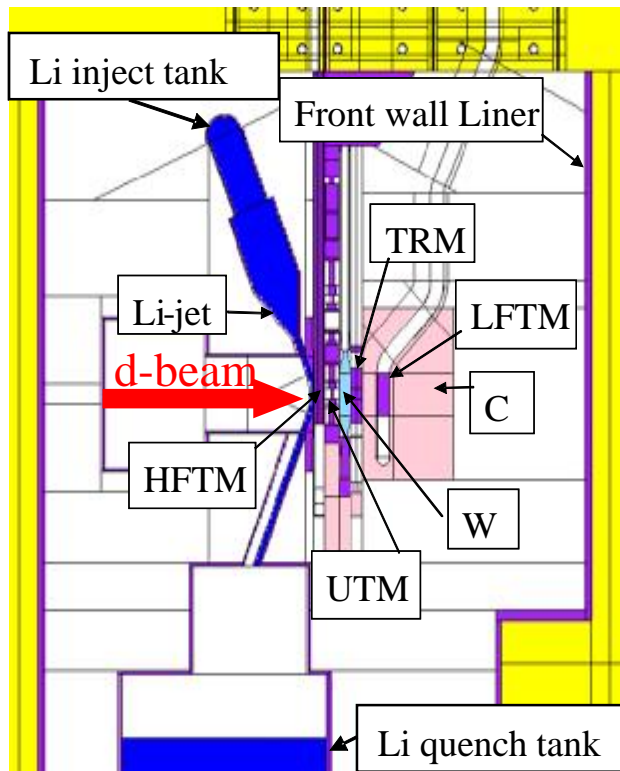
Calculated neutron spectra at different spots



**Neutronics calculations do predict smoothed (no peaks) energy distribution all over the IFMIF test cell**

## Li-jet nuclear responses: Tritium and Be-7 Inventories

### Test Cell & Li-loop



### $^3\text{H}$ and $^7\text{Be}$ production rates in Li-loop sub-systems (calculated by the McDeLicious code)

Loop component	Mass, kg	Reaction	Inventory	Rate, g/fpy
Li jet	1	$d + \text{Li}$	$^7\text{Be}$	1.5
		$d + \text{Li}$	$^3\text{H}$	6.0
		$n + \text{Li}$	$^3\text{H}$	0.4
Li injection tank	18	$n + \text{Li}$	$^3\text{H}$	0.2
Li quench tank	1200	$n + \text{Li}$	$^3\text{H}$	1.0
Li drain tubes	3	$n + \text{Li}$	$^3\text{H}$	0.1
<b>Total</b>			$^3\text{H}$	<b>7.7</b>

*D-Li collision in jet is a main source of Tritium and Be-7 inventories in the Li-Loop*

S.P. Simakov et al., JNM 329-333(2004)213

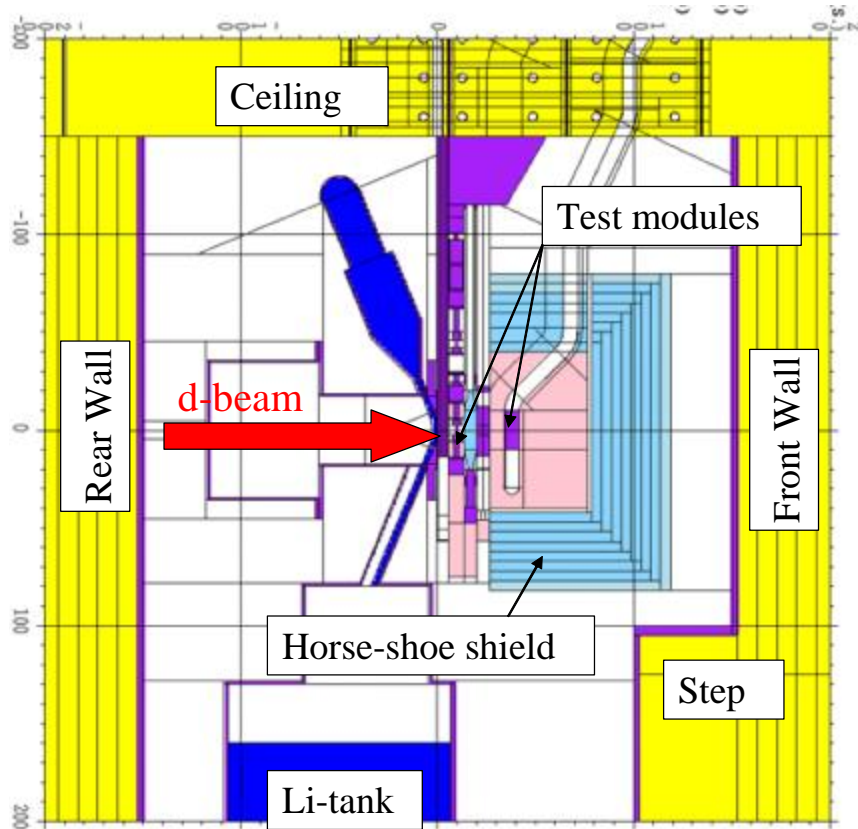
**MCNP geometry model**  
for the IFMIF test cell  
/latest version - md34/

developed by F. Wasastjerna  
*VTT Processes, Helsinki, Finland*

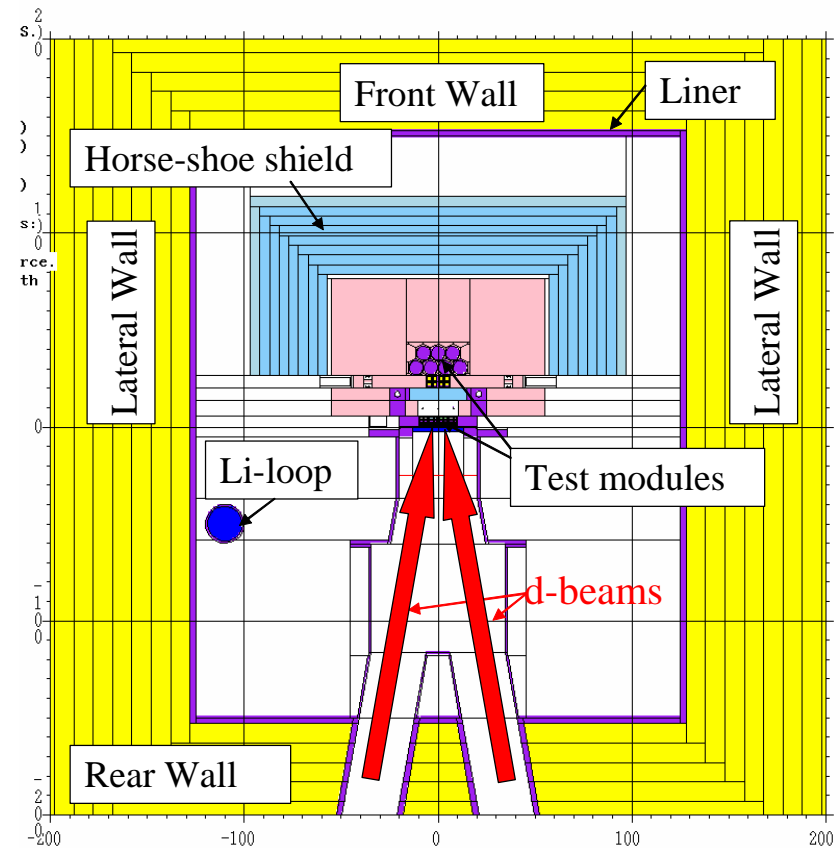
*F. Wasastjerna, Ann. of Nucl. Energy 35(2008)438–445*

# MCNP geometry Model

## Test Cell /Vertical cut/

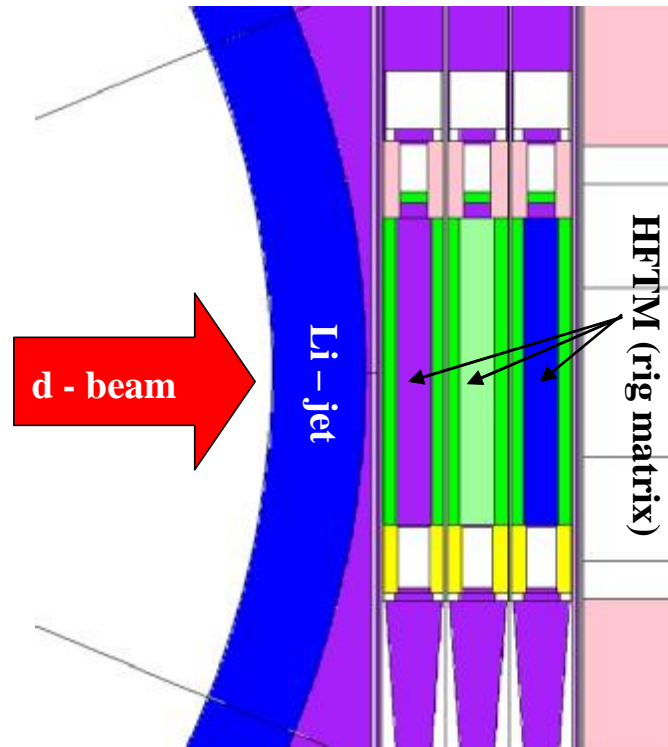


## Test Cell /Horizontal cut/

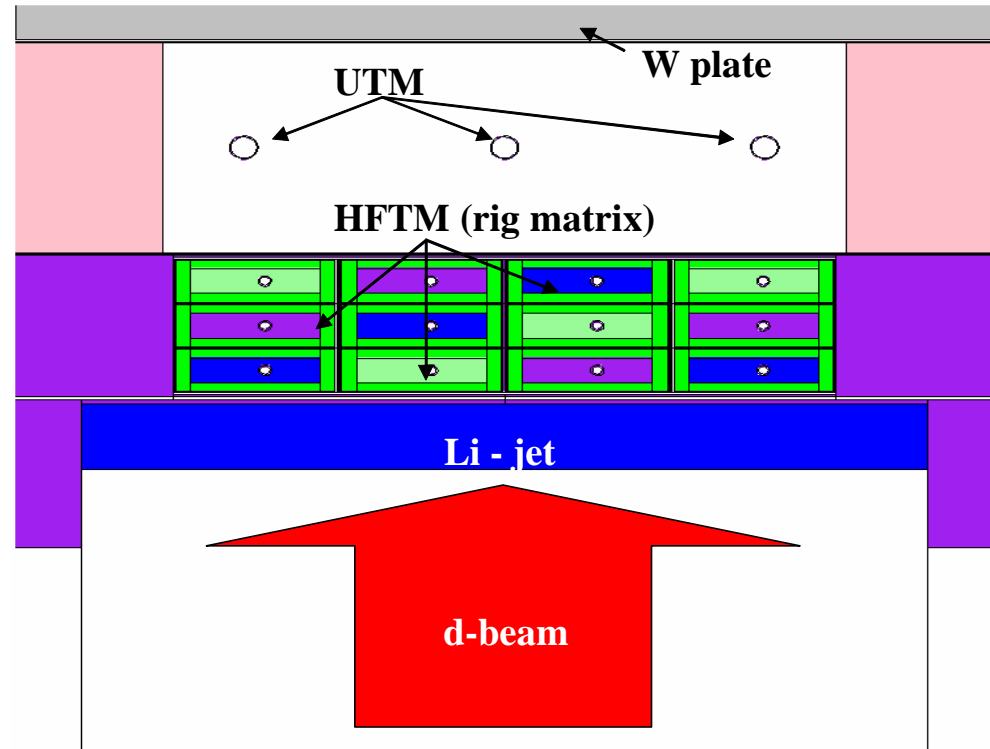


## MCNP geometry Model (continued)

HFTM /Vertical cut/

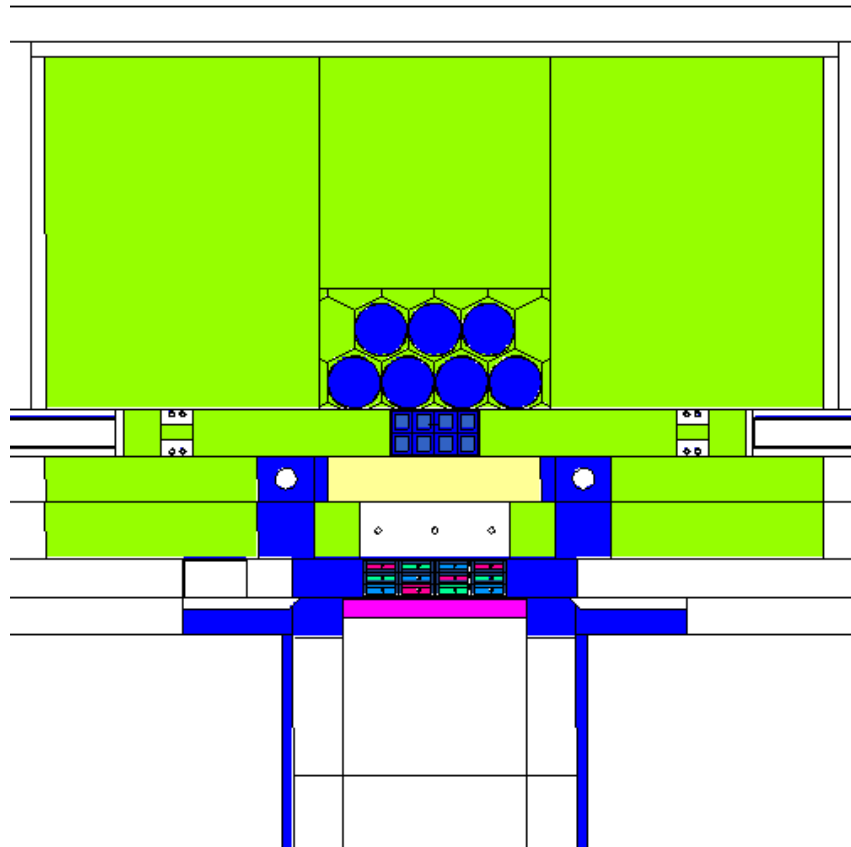


HFTM, MFTM, LFTM /Horizontal cut/

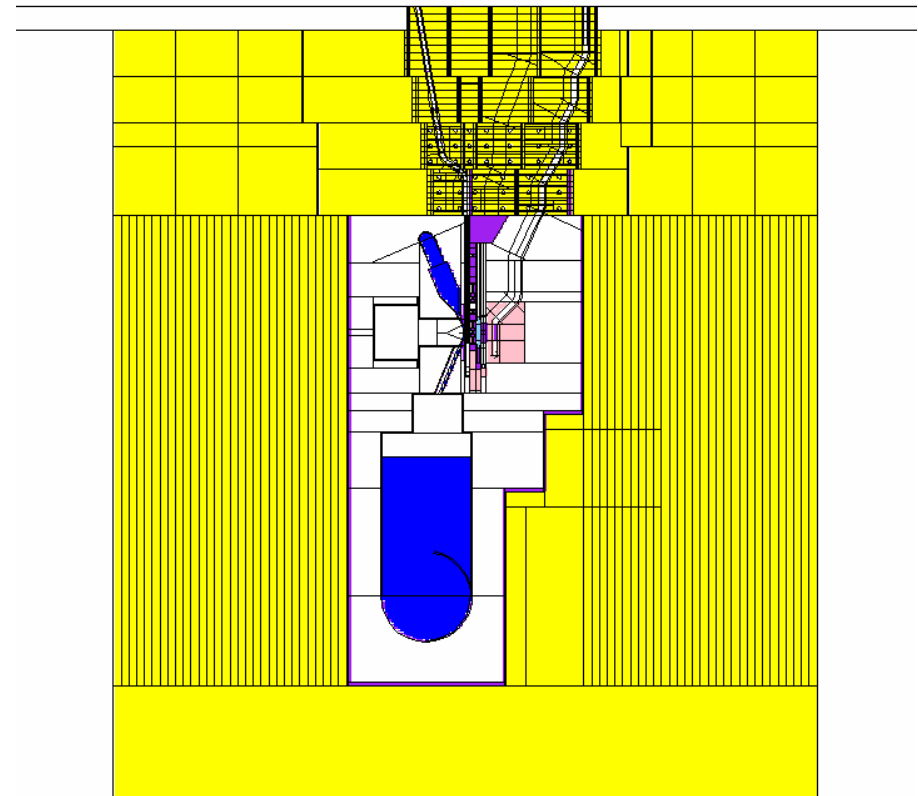


## MCNP geometry Model (continued)

HFTM, MFTM, LFTM /Horizontal cut/



Test Cell and Walls /Vertical cut/



## **Evaluated cross sections data**

for neutron transport and  
nuclear responses calculations  
in the IFMIF

## Neutron Cross-Sections $E \leq 20$ MeV - General purpose data ENDF evaluations -

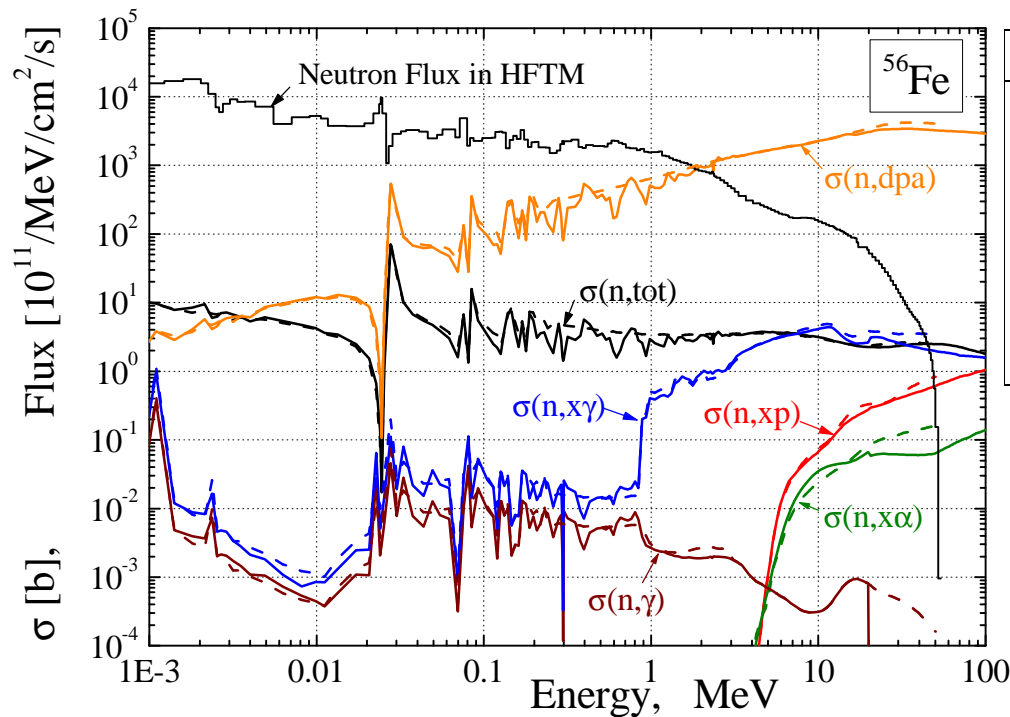
- IFMIF project
  - $^1\text{H}$ ,  $^{56}\text{Fe}$ ,  $^{23}\text{Na}$ ,  $^{39}\text{K}$ ,  $^{28}\text{Si}$ ,  $^{12}\text{C}$ ,  $^{52}\text{Cr}$ ,  $^{51}\text{V}$ ,  $^{6,7}\text{Li}$ ,  $^9\text{Be}$  (INPE/FZK)
  - $^{180,182-184,186}\text{W}$ ,  $^{181}\text{Ta}$  (EFF/JEFF)
- LANL 150 MeV data files (ENDF/B-VI.6 or B-VII)
  - $^{1,2}\text{H}$ ,  $^{12}\text{C}$ ,  $^{16}\text{O}$ ,  $^{14}\text{N}$ ,  $^{27}\text{Al}$ ,  $^{28,29,30}\text{Si}$ ,  $^{31}\text{P}$ ,  $^{40}\text{Ca}$ ,  $^{50,52,53,54}\text{Cr}$ ,  $^{54,56,57,58}\text{Fe}$ ,  $^{58,60,61,62,64}\text{Ni}$ ,  $^{63,65}\text{Cu}$ ,  $^{93}\text{Nb}$ ,  $^{182,183,184,186}\text{W}$ ,  $^{196,198, 199, 200, 201, 202, 204}\text{Hg}$ ,  $^{206, 207, 208}\text{Pb}$ ,  $^{209}\text{Bi}$
- NRG evaluations
  - $^{40,42-44,46,48}\text{Ca}$ ,  $^{45}\text{Sc}$ ,  $^{46-50}\text{Ti}$ ,  $^{54,56-58}\text{Fe}$ ,  $^{70,72-74,76}\text{Ge}$ ,  $^{204,206-208}\text{Pb}$ ,  $^{209}\text{Bi}$
- JENDL-HE data file
  - $^1\text{H}$ ,  $^{12,13}\text{C}$ ,  $^{14}\text{N}$ ,  $^{16}\text{O}$ ,  $^{24-26}\text{Mg}$ ,  $^{27}\text{Al}$ ,  $^{28-30}\text{Si}$ ,  $^{39,41}\text{K}$ ,  $^{40,42- 46,48}\text{Ca}$ ,  $^{46-50}\text{Ti}$ ,  $^{51}\text{V}$ ,  $^{50,52-54}\text{Cr}$ ,  $^{55}\text{Mn}$ ,  $^{54,56-58}\text{Fe}$ ,  $^{59}\text{Co}$ ,  $^{58,60-62,64}\text{Ni}$ ,  $^{63,65}\text{Cu}$ ,  $^{64,66-68,70}\text{Zn}$ ,  $^{90- 92,94,96}\text{Zr}$ ,  $^{93}\text{Nb}$ ,  $^{180,182-184,186}\text{W}$ ,  $^{196,198-202,204}\text{Hg}$
- Few other evaluations
  - KAERI ( $^{12}\text{C}$ ,  $^{27}\text{Al}$ ,  $^{56}\text{Fe}$ ,  $^{208}\text{Pb}$ ), BNL ( $^{12}\text{C}$ ,  $^{56}\text{Fe}$ ,  $^{208}\text{Pb}$ ,  $^{209}\text{Bi}$ ), IPPE ( $^{232-238}\text{U}$ ,  $^{237,239}\text{Np}$ ,  $^{236-244}\text{Pu}$ )



# Transport cross sections and nuclear responses

Evaluated neutron cross sections  
(LANL – solid, INPE/FZK – dash)

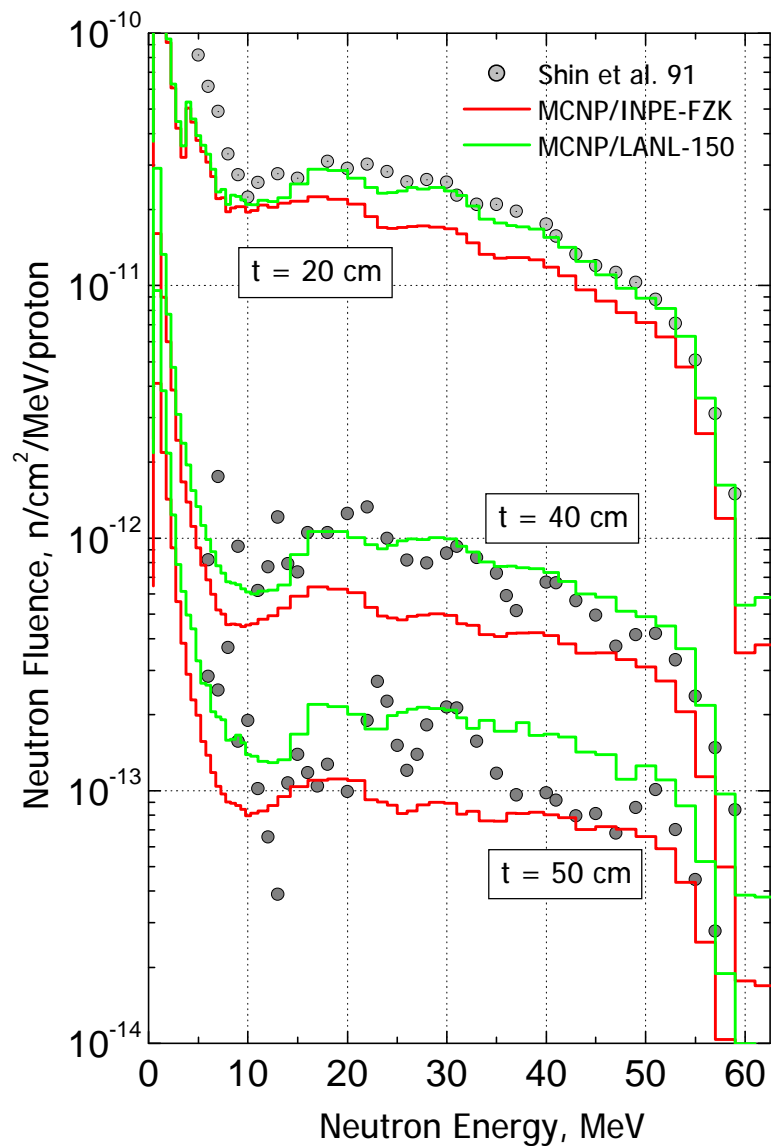
Responses in HFTM/IFMIF vs. Libraries  
(uncertainties due to XS data)



Parameter	LANL	INPE	Differ.
dpa-rate, 1/fpy	31.1	33.6	8 %
Heating, W/cm3	16.9	19.7	16 %
H-production, appm/fpy	1602	1767	10 %
He-production, appm/fpy	345	396	13 %
n-flux, $10^{14}$ /cm2/s	7.05	7.43	5 %
$\gamma$ -flux, $10^{14}$ /cm2/s	3.38	3.59	6 %

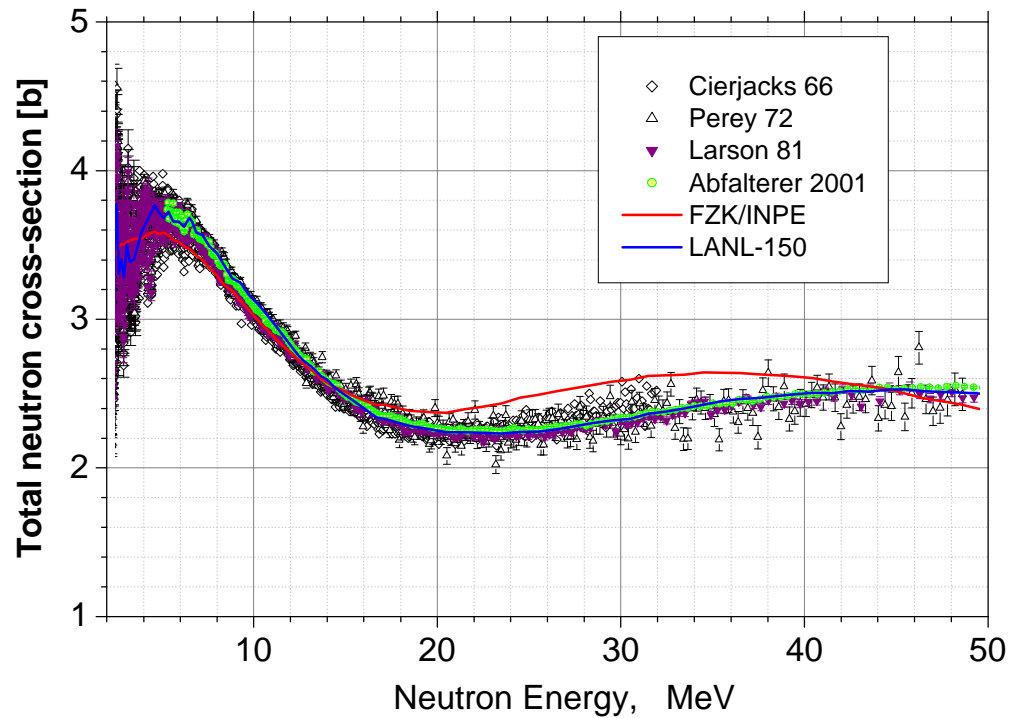
*Expected uncertainties of IFMIF nuclear responses due to the transport cross sections data amounts at least (5 - 15)%*

# Iron Transmission Benchmark Experiment



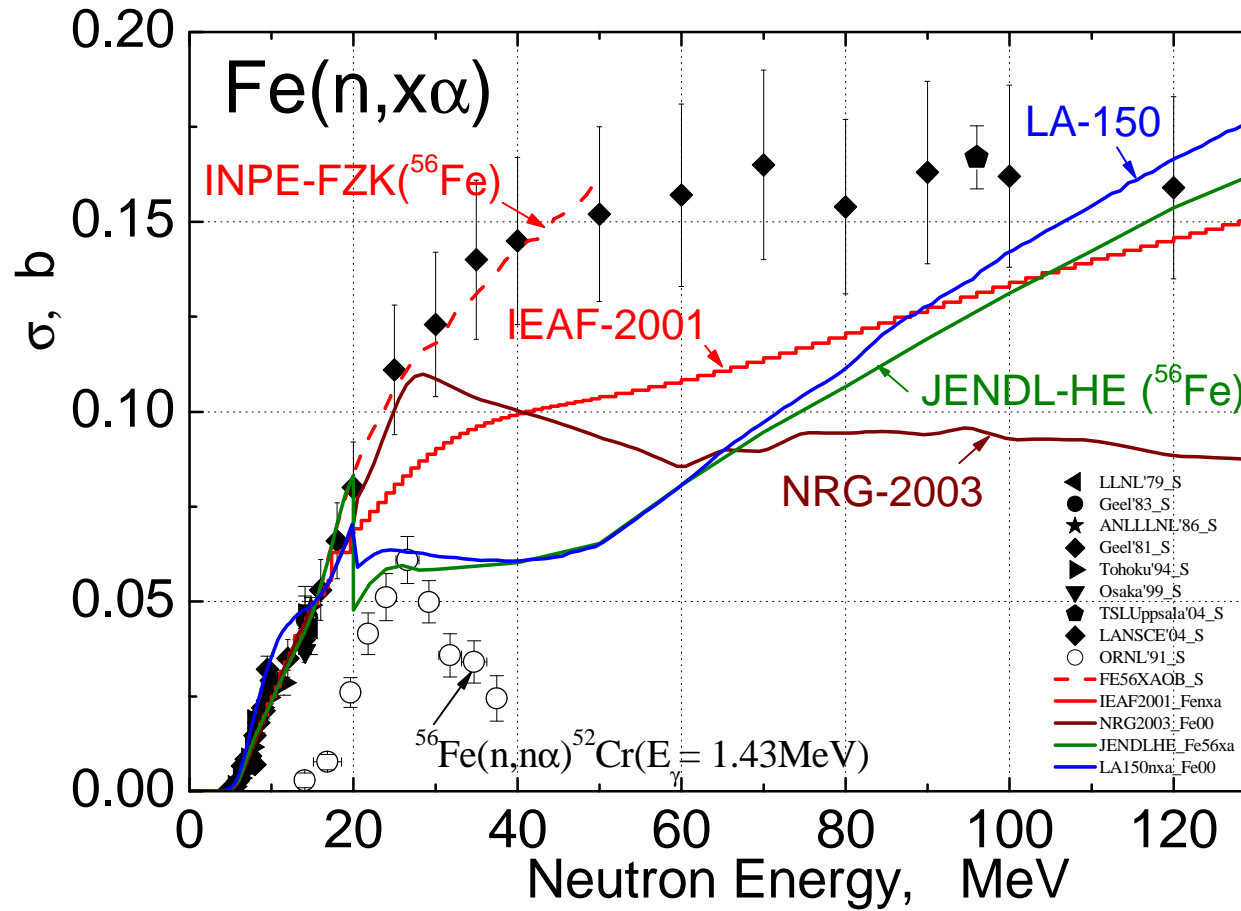
*Fe slabs (20, 40 50 cm) irradiated with source neutrons produced by 65 MeV protons on Cu target /TIARA, Shin et al./*

*Fe(nat) total neutron cross-section*



*LA-150 looks more preferable than INPE-FZK*

## Gas (He) production cross-sections in Iron



*INPE-FZK looks more preferable than LA-150 (!?)*

# Transport and nuclear response cross sections files for IFMIF

## High Energy Files (up to 150 MeV)

LA-150 library (extension = 24c), xsdir = iedirLA

n + 1-H-1, H-2

n + 4-Be-9

n + 6-C-nat

n + 8-O-16

n + 13-Al-27

n + 14-Si-28, Si-29, Si-30

n + 20-Ca-nat

n + 24-Cr-50, Cr-52, Cr-53, Cr-54

n + 26-Fe-54, Fe-56, Fe-57

n + 28-Ni-58, Ni-60, Ni-61, Ni-62, Ni-64

n + 29-Cu-63, Cu-65

n + 74-w-182, W-183, W-184, W-186

## Fusion Energy Files (up to 20 MeV)

JENDL-FF library (extension = 41c)

n + 22-Ti-46, Ti-47, Ti-48, Ti-49, Ti-50

(better to replace by JEFF-3.1, < 200 MeV)

ENDF/B-VI library (extension = 60c)

n + 16-S-32

(better to replace by ENDF/B-VII, < 20 MeV)

## IFMIF Energy domain Files (up to 50 MeV)

INPE/FZK library (extension = 95c)

n + 3-Li-6, Li-7 from file wq\_Li6 and wq\_Li7 (xsdir\_wq\_Li6\_Li7)

n + 11-Na-23 from file iexs2 (bin) or iexs1 (ASCII, xsdir =iedir1)

n + 19-K-39 ...

n + 23-V-51 ...

# **McDeLicious:**

programming details

## McDeLicious Logic Structure

### 1. Main subroutine **source lib-05.F90** does following:

- calls subroutine **load**(filename,..) which uploads in memory the ACE files with d-<sup>6</sup>Li and d-<sup>7</sup>Li cross sections
- reads beam parameters from the McDeLicious input file such as number of beams, declination angle, d-beam spatial profile parameters, deuteron incident energy, Li-jet density, entrance surface and target cell
- calls subroutine **yield\_Ed**(..) which calculates deuteron range in Li media, total neutron yield and prepares the tables for deuteron track sampling

for the First sampling history

## McDeLicious Logic Structure (continued)

for All others sampling histories

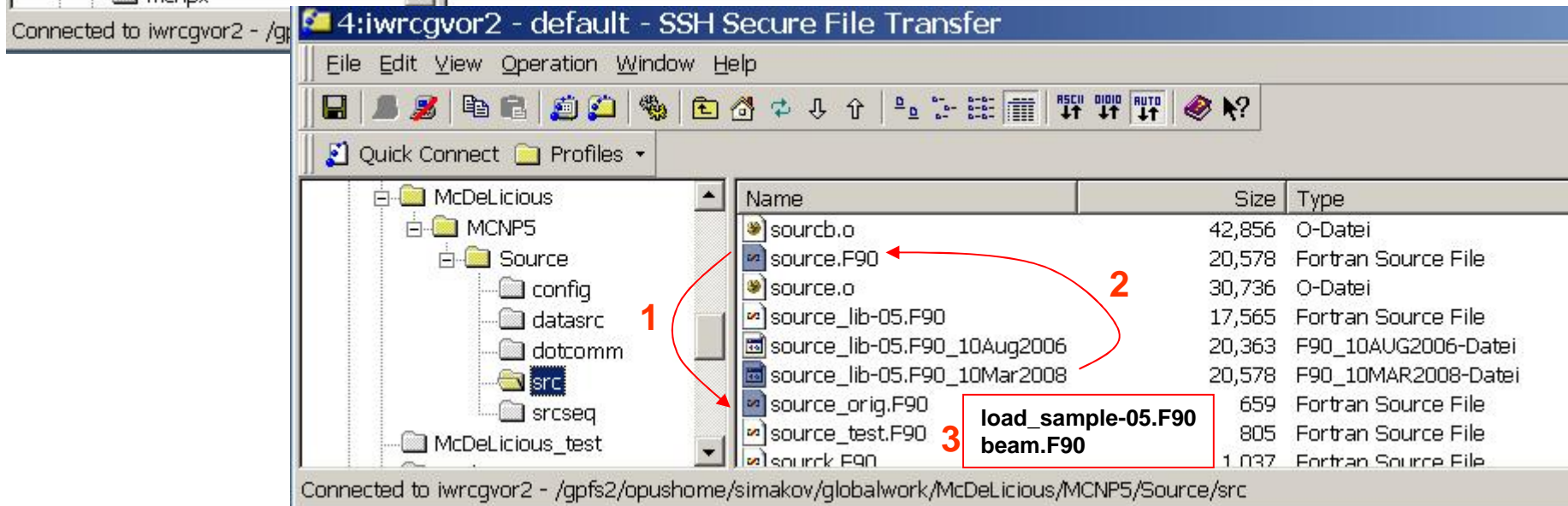
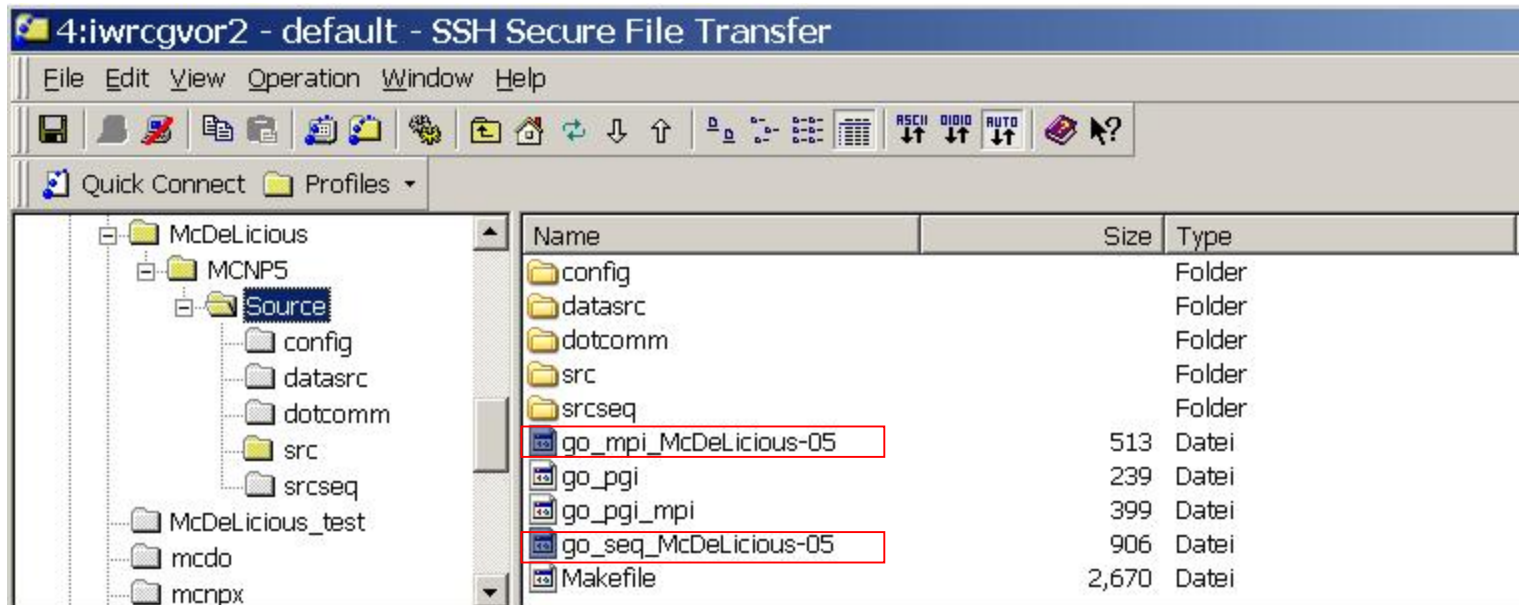
- calls subroutine **yz\_sample(...)** and samples deuteron direction and entrance point on the surface of Li target
  - calls subroutine **sample\_Ed(...)**, which samples d-track length to collision and calculates this point  $(X, Y, Z)$ , deuteron energy  $E_d$  and neutron weight  $W_n$  there
  - samples whether isotope  ${}^6\text{Li}$  or  ${}^7\text{Li}$  a deuteron collides with
  - subroutine **sample\_EnAng (...)** – samples neutron emission Energy  $E_n$ , polar  $\Theta_n$  and azimuth  $\varphi_n$  Angles using tables from d-Li ACE file
  - submits to MCNP parameters of generated neutron:  
 $\{X, Y, Z\}, \{\cos_x, \cos_y, \cos_z\}, E_n, W_n, T_n=0$
2. Files **load\_sample-05.F90** and **beam.F90** collect subroutines and functions mentioned above: *load, yield\_Ed, sample\_Ed, sample\_EnAng, dedx, f\_average, yz\_sample, gausdev*

## McDeLicious subroutines allocation and compilation with MCNP5 ones to get executable for *mpi* parallelism

- Ø Subroutine **source\_lib-05.F90** should replace MCNP dummy subroutine **source.F90** in directory MCNP5/Source/src; files **load\_lib-05.F90** and **beam.F90** should be allocated there too
- Ø System dependent script for MCNP5 compilation **go\_pgi\_mpi** (after slight modification - **go\_mpi\_McDeLicious-05**) should be available in directory MCNP5/Source and has to be executed
- Ø After successful compilation an executable file **mcnp5.mpi** will be produced which should be renamed to **McDeLicious-05** and moved in your working or bin directory
- Ø To run McDeLicious code one needs specific ACE files :  
**d\_li6\_056.ace\_up50** and **d\_li7\_056.ace\_up50**  
- which are the d-<sup>6,7</sup>Li evaluation processed by NJOY code



# McDeLicious subroutines allocation in MCNP5 directories



## McDeLicious Input File Structure

MCNP cards

```
message:Datapath=~/.directory_for_data
xmdir=xmdir_file_for_cross_sections
```

```
empty line
Cell cards
empty line
Surface cards
empty line
Materials
```

```
Sp901
....
SP916
```

MCNP cards

```
Tally cards
F6n,p cell_number
....
```

```
mode n,p
phys:p j 1
cut:n 1j 5.0E-7
nps 1.E+7
```

IFMIF Test Cell geometry  
and materials cards  
(around lines 8000 lines)

D-Li source specification cards  
(see next slide)

Responses specification cards  
(see next slide)

Problem specification cards

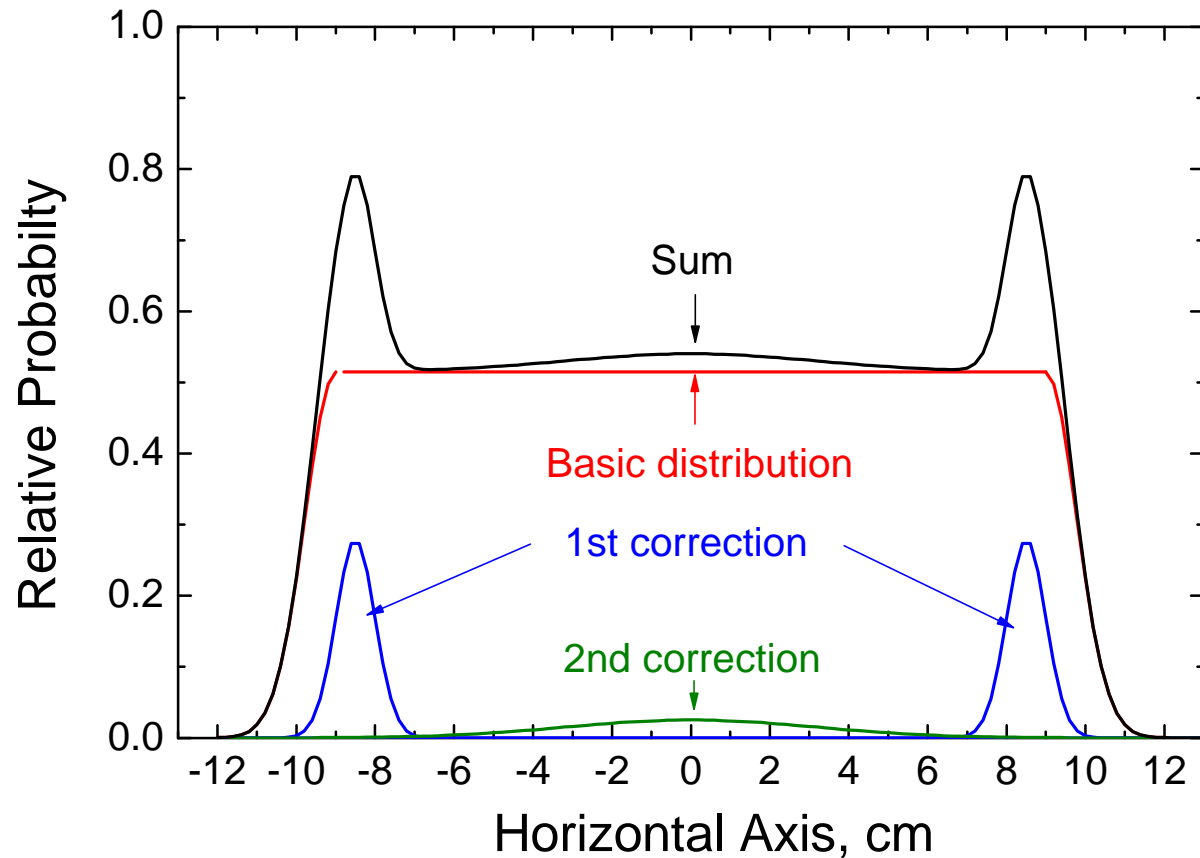
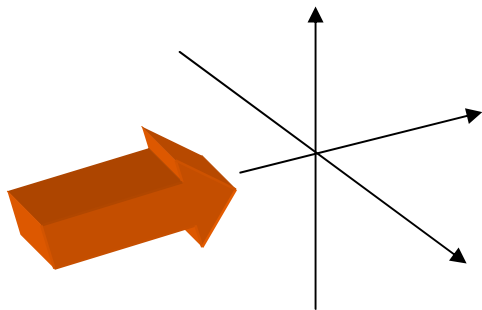
## McDeLicious Input File: D-Li Source Specification

```

C -----
c  two 40MeV d-beams declined in Horizontal plane by 10deg, 20x5cm2 Footprint
C -----
c  beams      #1          # 2
SI901 L      1          1          $ target number
SI902 L      1          1          $ beams current (only relative value has meaning)
SI903 L     40         40         $ beams energy Ed [MeV]
c           cos(x) cos(y) cos(z)   cos(x) cos(y) cos(z) for beam orientation
SI904 L 0.173648 0. 0.984808 -0.173648 0. 0.984808 $ beams 10deg in Horiz.
SI905 L 1 0 0      1 0 0          $ beam orientation vector: along X-axis
c           Xo   σ   m   Xo   σ   m   for beam spatial profile for 20 x 5 cm**2
SI906 L 9.0 0.6 1.00 9.0 0.6 1          $ basic horizontal parameters
SI907 L 2.0 0.6 1.00 2.0 0.6 1          $ basic vertical parameters
SI908 L 8.5 0.25 0.35 8.5 0.25 0.35     $ first horizontal correction
SI909 L 0 0 0      0 0 0          $ first vertical correction
SI910 L 0 10 0.2   0 10 0.2         $ second horizontal correction
SI911 L 0 0 0      0 0 0          $ second vertical correction
c           x   y   z      x   y   z   for beam centre coordinates
SI912 L 0 0 -2.68   0 0 -2.68       $ beam spot centre [cm] on Li-jet surface
SI913 L 2001          $ program cell number for Li-jet
SI914 L 0 0 1          $ target surface normal: along Z-axis
SI915 L 0.512 2.50    $ target density [g/cm**3], thickness [cm]
SI916 L 0.075 0.925  $ Li-6 and Li-7 relative Abundance

```

# One d-beam spatial profile presentation



$$p(x) = m * \exp(-(x - x_0)^2 / 2s) / \sqrt{2ps} \quad (+ \text{Heaviside function for basic profile})$$

	Horizontal			Vertical		
	m	X <sub>0</sub> , cm	σ, cm <sup>2</sup>	m	X <sub>0</sub> , cm	σ, cm <sup>2</sup>
Basic	1.00	±9.0	0.60	1.0	±2.0	0.6
1st correction	0.35	±8.5	0.25	-	-	-
2nd correction	0.20	0.0	10.0	-	-	-

P. Wilson, Report FZKA 6218, 1999

## Tallies and its normalization

### Overall normalization

- All McDeLicious results (talleis) are normalized per one incident deuteron

### Specific Tally normalization:

- Flux Tally (F4, F5) for Neutron and Photon [1/cm<sup>2</sup>/s]:

$$I \text{ [mA]} * 1.E-3 / (e^- = 1.60218E-19) = 6.2415E+15 * I \text{ [mA]} = 1.56045E+18 \text{ (I=250 mA)}$$

- Heating Tally (F6:n,p) by neutrons and photons [W/g]:

$$I \text{ [mA]} * 1.E-3 \text{ (MeV/J=1.60218E-13)} / (e^- = 1.602177E-19 \text{ C}) = I \text{ [mA]} * 1.E+3 = 2.5E+5 \text{ (I=250mA)}$$

- Heating in material M using mean flux in Cell estimated by tally F4 [W/g]:

F4:n cell

FM4 I [mA] \* 1.E+3 \* atom/gramm\_denisity M -1 -4

F4:p cell

FM4 I [mA] \* 1.E+3 \* atom/gramm\_denisity M -5 -6

## Tallies and its normalization (continued)

### Displacement Damage Rate caused by neutrons in materials

$$\text{Damage\_Rate} [dpa/ fpy] = F [n/cm^2/s] \times S_{dpa} [b] \times 1.E - 24 [cm^2 / b] \times 3.1557E + 7 [s/ fpy]$$

where:

$F [n/cm^2/s]$  - neutron flux =  $F4 [n/cm^2] * I [mA] * 1.E-3 / (e- = 1.602177E-19 C)$

$S_{dpa} [b] = 0.8 \times DE [b * MeV] / (2 \times E_d [eV])$  - displacement cross section

$DE [MeV*b]$  - damage energy (available in MT=444)

$E_d [eV]$  - threshold energy to displace atom in lattice (e.g., 40 eV for Fe)

Finally:

$$\text{Damage\_Rate} [ dpa/ fpy ] = (78785.2 / E_d \times I [mA]) \times F4 [ n/cm^2 ]$$

Example: dpa/fpy in Iron (material M) which fills the Cell;  
d-beam current  $I = 250$  mA

F4:n Cell

FM4 4.9241E+5 M 444

## Tallies and its normalization (continued)

Gas production rate = gas atoms per 1 target atom over time unit

$$\begin{aligned} \text{Gas\_Production} [\text{appm}/\text{fpy}] &= \\ &= F[\text{n}/\text{cm}^2/\text{s}] \times \sigma_{\text{gas}}[\text{b}] \times 1.E-24[\text{cm}^2/\text{b}] \times 3.1557E+7[\text{s}/\text{fpy}] \times 1.E+6[\text{appm}] \end{aligned}$$

where:

$F$  [n/cm<sup>2</sup>/s] - neutron flux =  $F4[\text{n}/\text{cm}^2] * I [\text{mA}] * 1.E-3 / (e- = 1.602177E-19 \text{ C})$   
 $\sigma_{\text{gas}}$  [b] - gas production cross-section MT=203 (H) or MT=207(He)

Finally:

$$\text{Gas\_Production}[\text{ appm}/\text{fpy} ] = ( 0.19696 \times I[\text{mA}] ) \times F4[ \text{n}/\text{cm}^2 ]$$

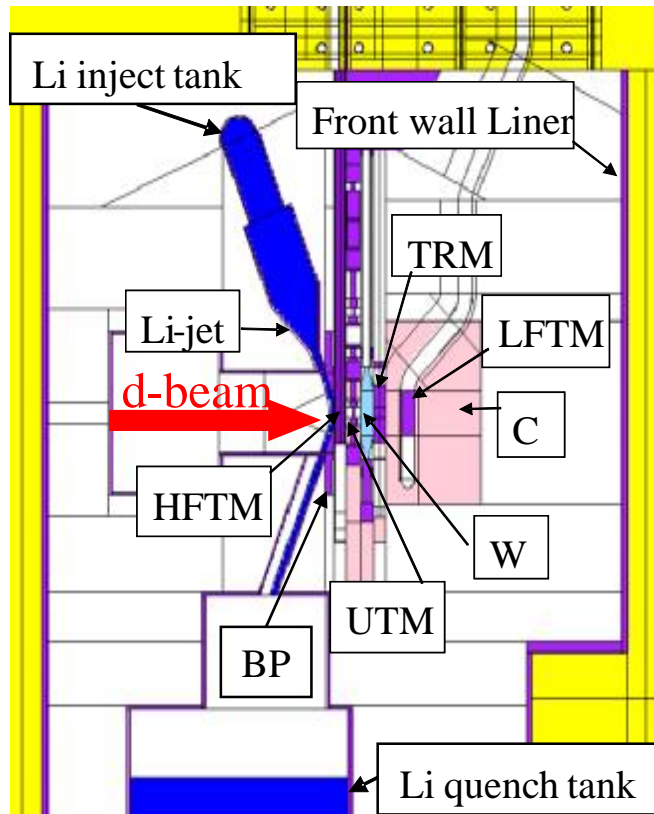
Example: He [appm/fpy] in Iron (material M) which fills the Cell;  
d-beam current I = 250 mA

F4:n Cell

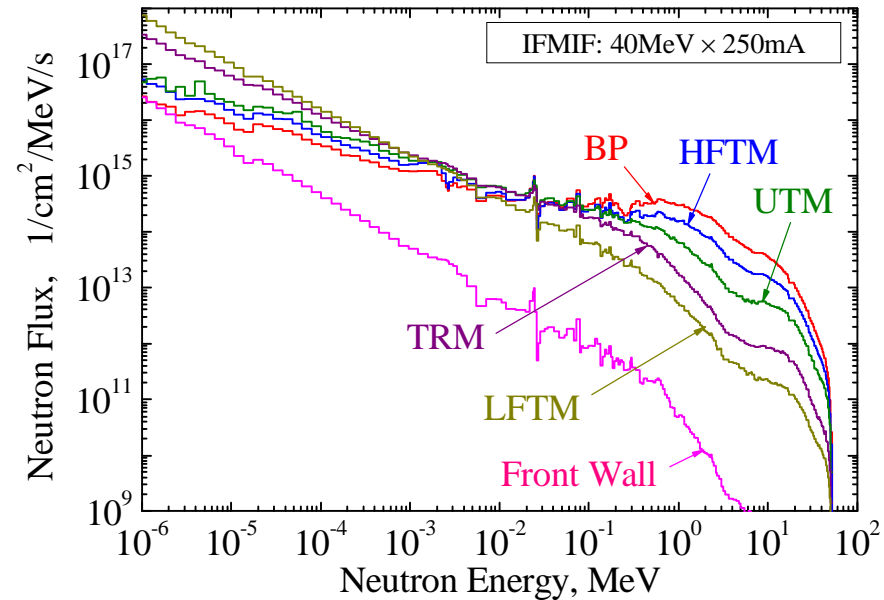
FM4 49.241 M 207

# Nuclear Responses in the IFMIF sub-systems

## Test Cell global model



## Neutron energy fluxes in the IFMIF



## Neutron fluxes & dpa in the IFMIF components

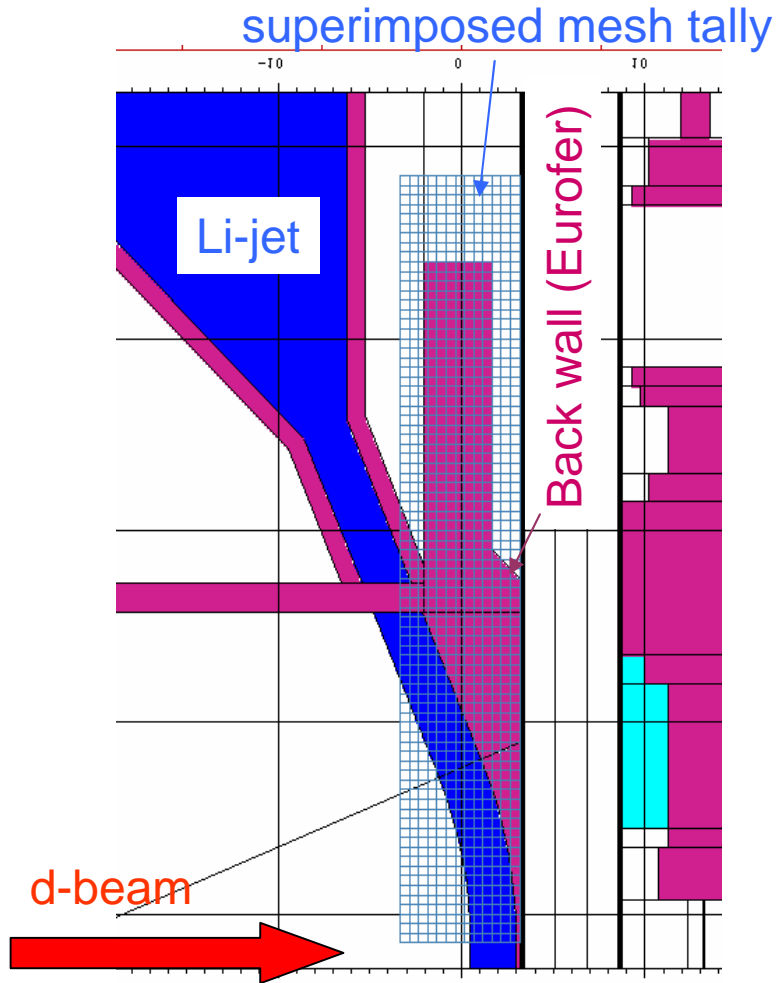
IFMIF test cell sub-system	Neutron Flux, $10^{14}$ n/cm <sup>2</sup> /s	Damage (Element), dpa/fpy
Li-jet back Plate (BP)	15.0	66 (Fe)
High Flux Test Module (HFTM)	7.3	20 - 55 (Fe)
Univers. Test Machine (UTM)	3.5	11 (Fe)
Tungsten Moderator (W)	2.0	1.1 (W)
Tritium Release module (TRM)	1.1	2.4 (Fe), 3.5 (Be)
Low Flux Test Module (LFTM)	0.61	0.65 (Fe)
Front wall steel liner	0.01	0.004 (Fe)

S.P. Simakov et al. *Fus.Eng.Des.*75-79(2005)813

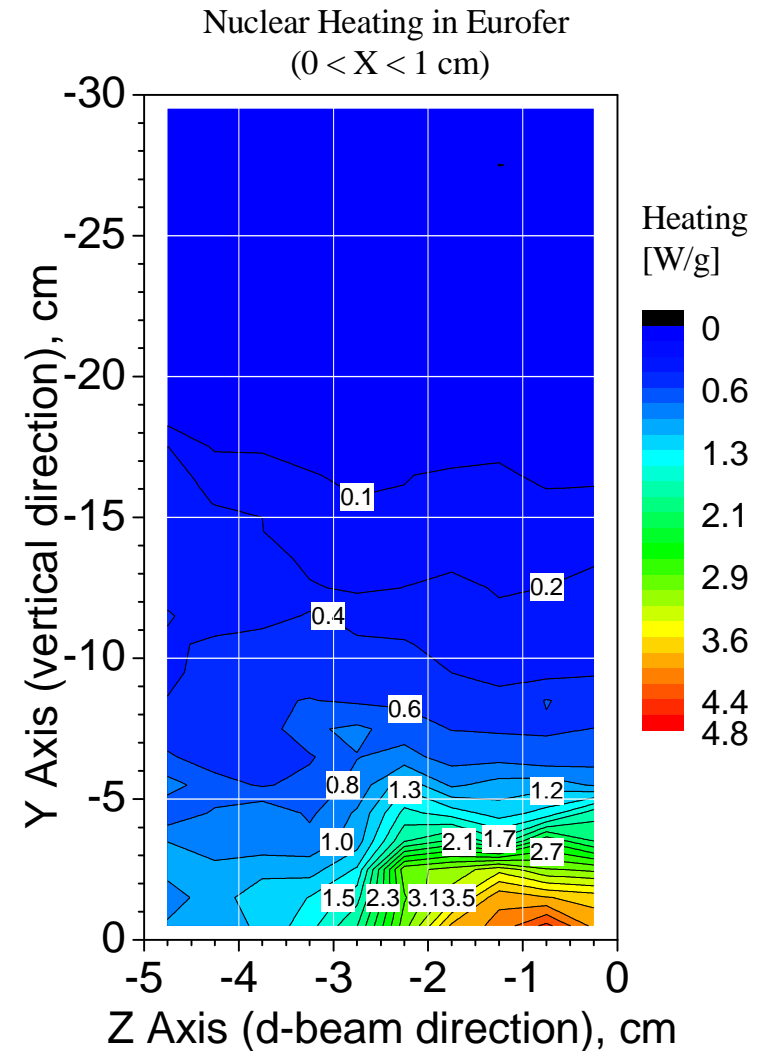


# Nuclear Responses in the IFMIF sub-systems /F4 mesh tallies capabilities/

Model fragment of Li-jet backed by Wall



Nuclear Heating in Eurofer from F4 mesh tally



**IFMIF neutronics, McDeLicious code  
Test Cell geometry model:**

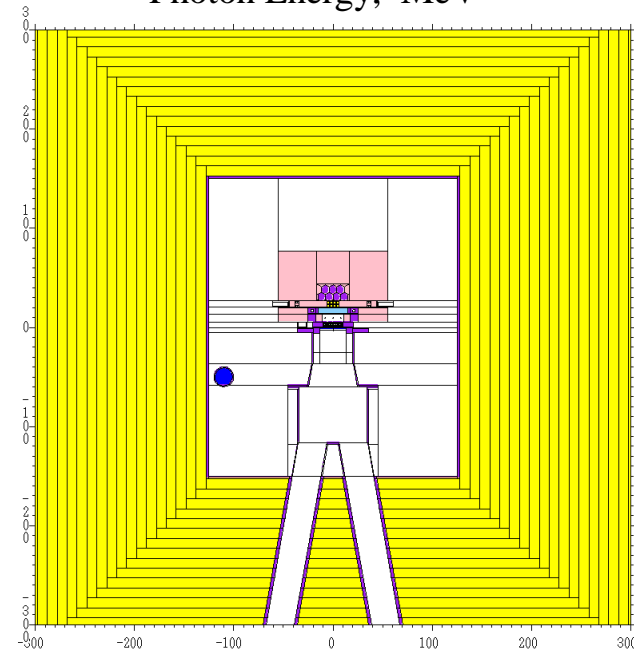
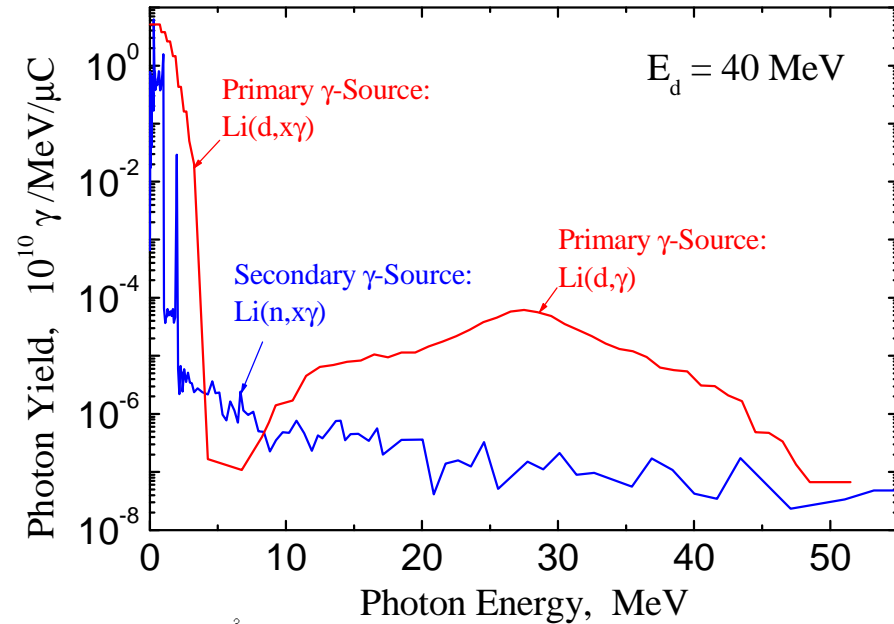
further developments

## McDeLicious further development

Direct Gamma-source:  
inclusion of  $\text{Li}(d,x\gamma)$  photons to account  
their contribution to the responses

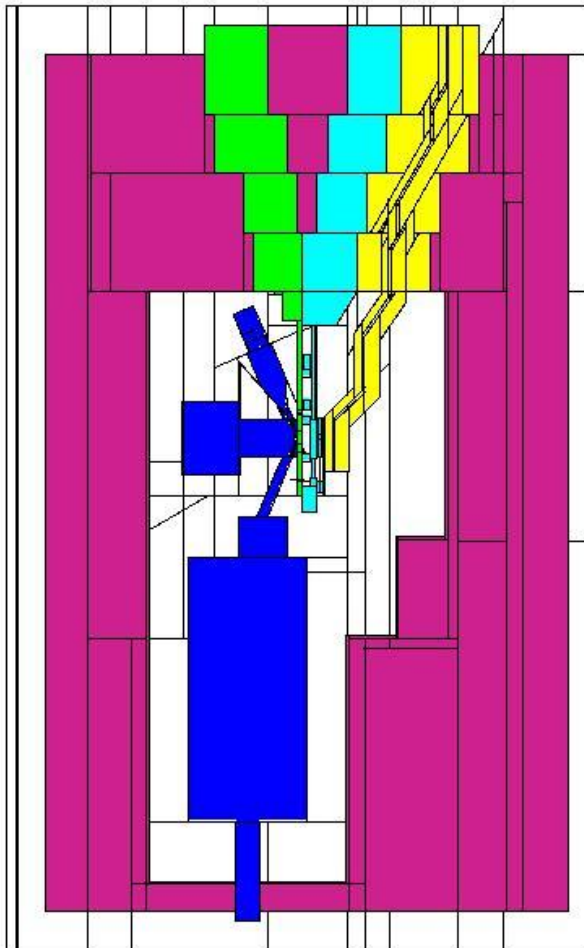
Variance reduction:  
biasing of d-Li source angular distribution  
to improve statistics for backward directions  
and for streaming through the shield

....

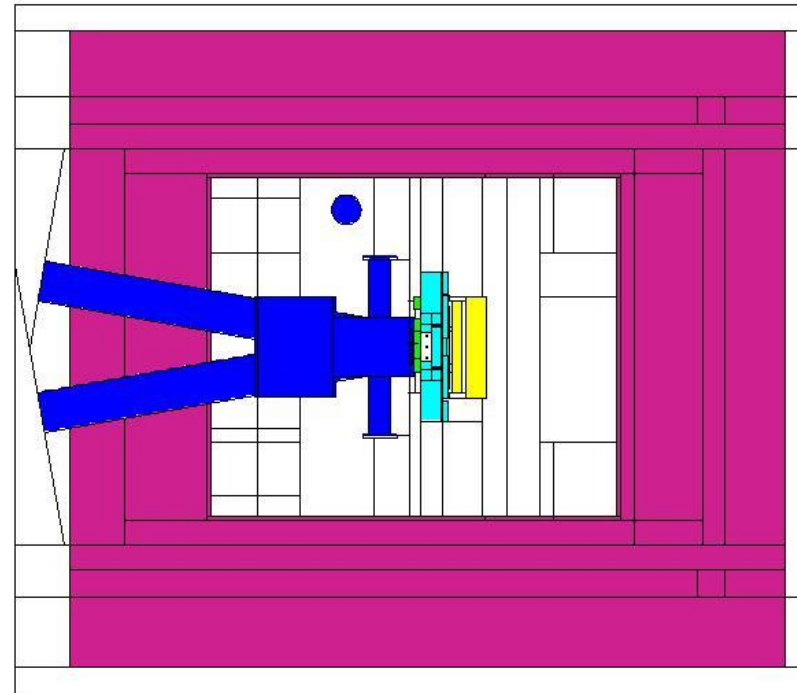


## IFMIF Test Cell MCNP Model converted by McCAD from CAD

Vertical cut of test cell



Horizontal cut at target mid-plane level



*H. Tsigé-Tamirat et al. Fus. Eng.Des.,82(2007)1956*